

# THEORY AND TESTING OF DUPLEXERS



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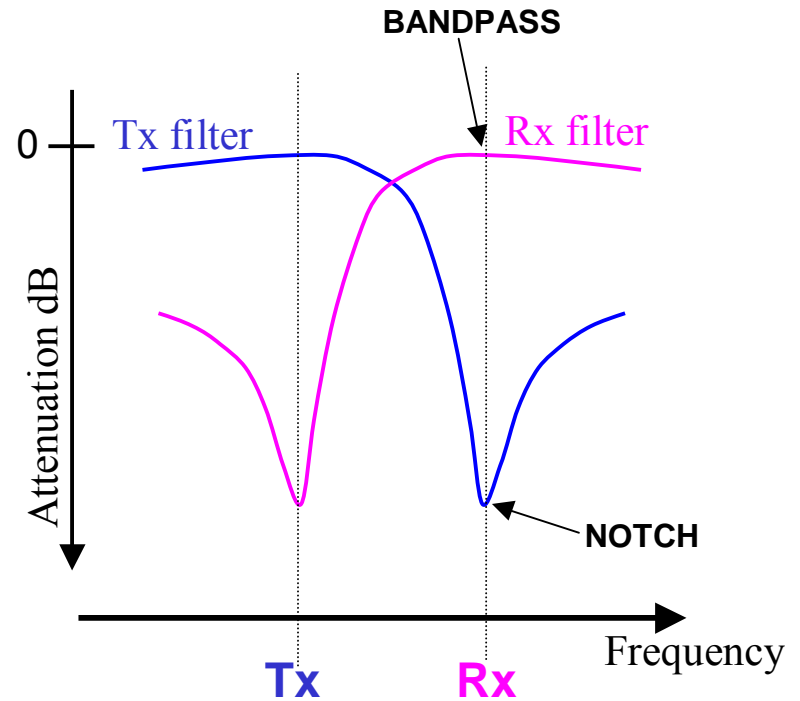
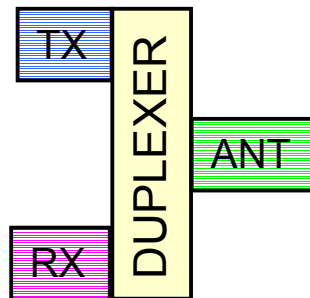
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- ❑ INTRO
- ❑ WHY USE DUPLEXERS ?
- ❑ BASIC TYPES OF DUPLEXERS
- ❑ SIMPLE LC MODELS FOR EACH TYPE
- ❑ ADJUSTMENT AND VERIFICATION
- ❑ PUTTING IT ALL TOGETHER - EXAMPLES
- ❑ PITFALLS
- ❑ REFERENCES

# WHY USE DUPLEXERS ?

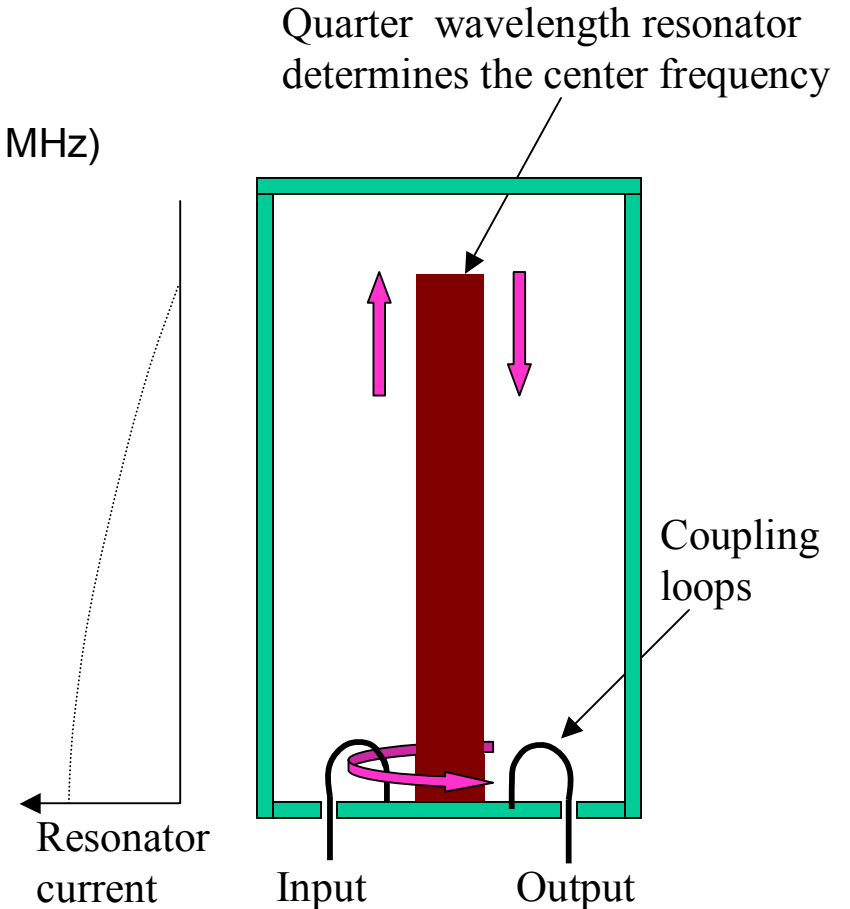
## DUPLEXERS...

- ❑ Allow simultaneous transmit and receive on the same antenna
- ❑ The Rx filter attenuates the TX signal ~ 75 dB or more (approx 30 million times) and vice-versa
- ❑ The Tx filter attenuates the TX broadband noise being fed into the Rx by a similar amount
- ❑ Three port devices:



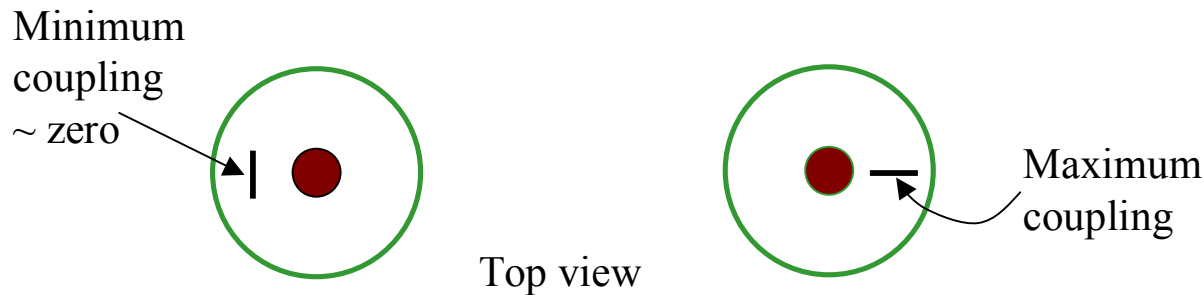
## CAVITIES IN GENERAL

- ❑ Use a very low loss transmission line to improve selectivity (high Q)  
(~0.08 dB loss / 100 ft for a 6 in. cavity @ 150 MHz)
- ❑ The resonator acts as a quarter wave antenna inside a closed box, with max. current at the base
- ❑ In – out loops magnetically couple energy to the resonator
- ❑ Capacitive coupling may also be used but not discussed here
- ❑ There is a 180 degree phase reversal between the in – out signals.



## LOOP COUPLING TO THE RESONATOR

- ❑ Loop orientation affects coupling:



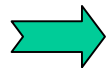
- ❑ Loop size: increasing the loop size increases coupling and its inductance as well
- ❑ Loop proximity from the resonator: placing the loop closer will increase coupling.
- ❑ Loop coupling affects the insertion loss and selectivity in the bandpass region and the notch frequency in notch-bandpass designs.

## BASIC TYPES OF DUPLEXERS

### TX – RX FREQ SEPARATION

LO – HI PASS FILTERS

WIDE



BANDPASS CAVITIES

MEDIUM

NOTCH – BANDPASS CAVITIES

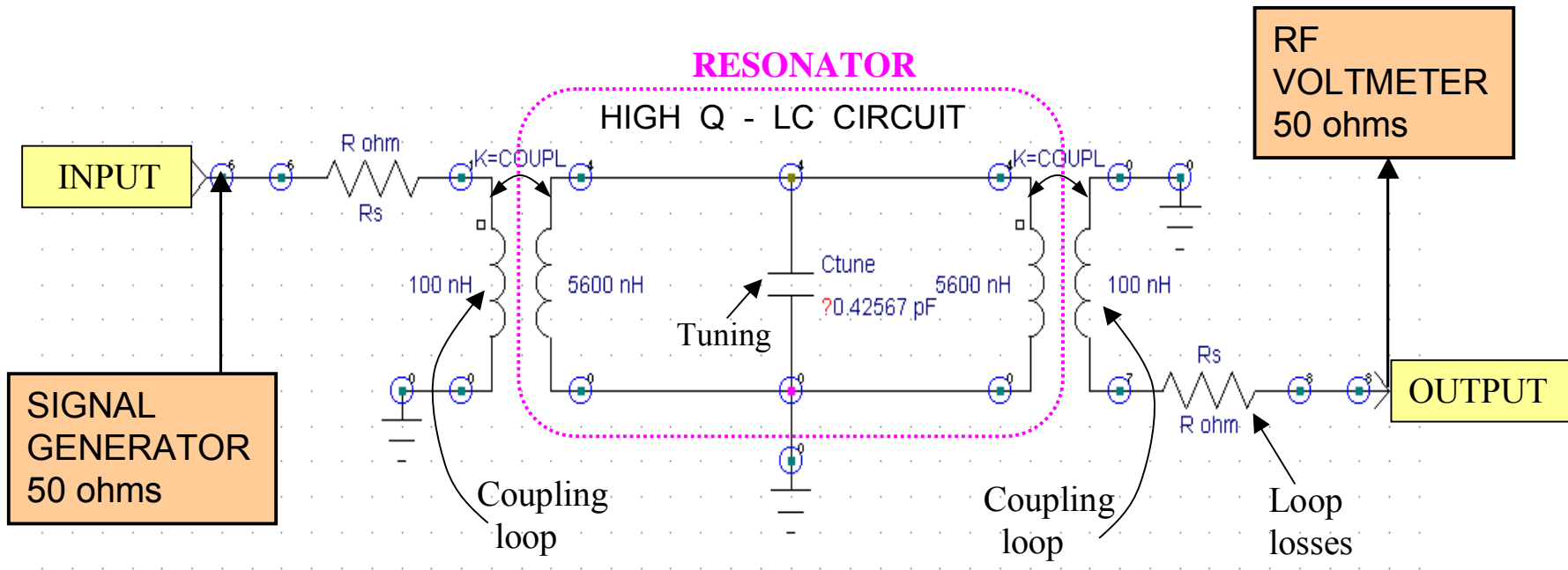
NARROW

NOTCH CAVITIES

NARROW

# BANDPASS CAVITIES

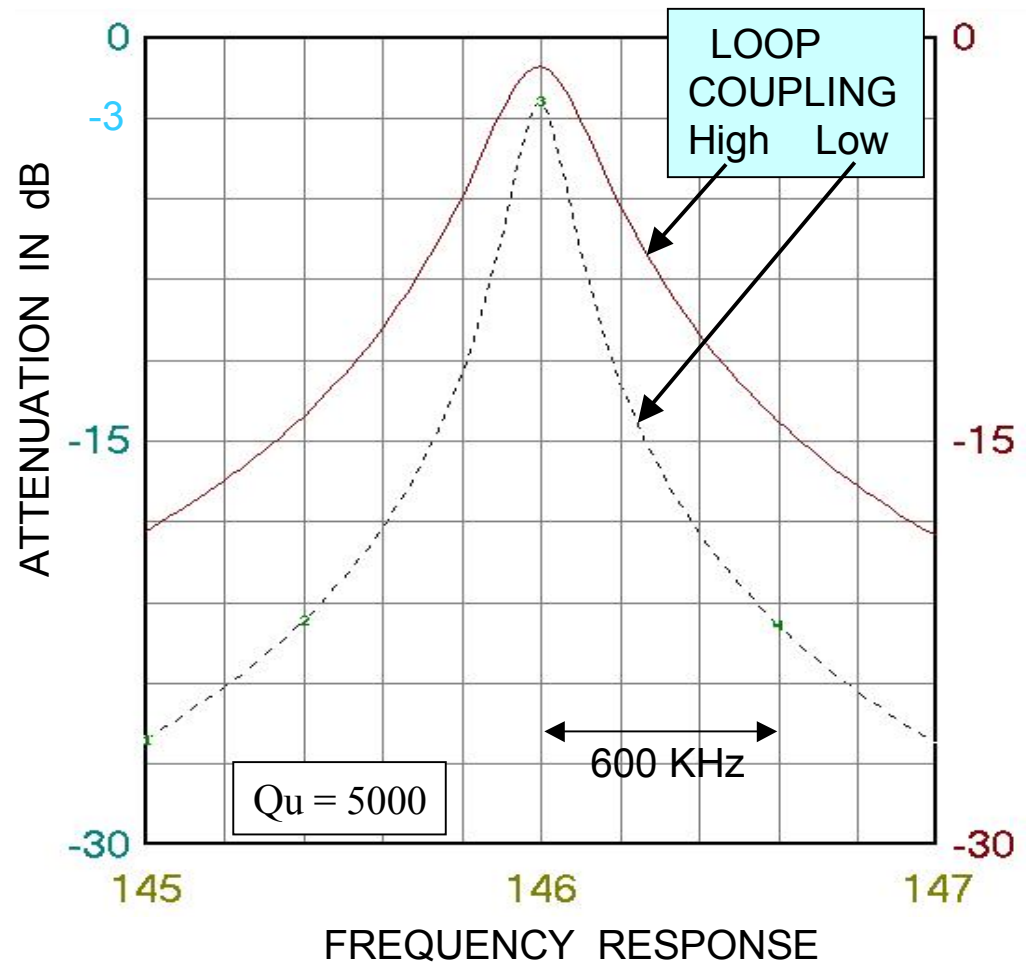
## EQUIVALENT CIRCUIT



- ❑ THE QUARTER WAVELENGTH RESONATOR IS MODELED WITH A HIGH Q - LC CIRCUIT
- ❑ TYPICAL RESONATOR  $Q_u$  VALUES: 2100 for 4 in. Cavity, 5000 for a 6 in. cavity

# BANDPASS RESONATOR RESPONSE CURVES

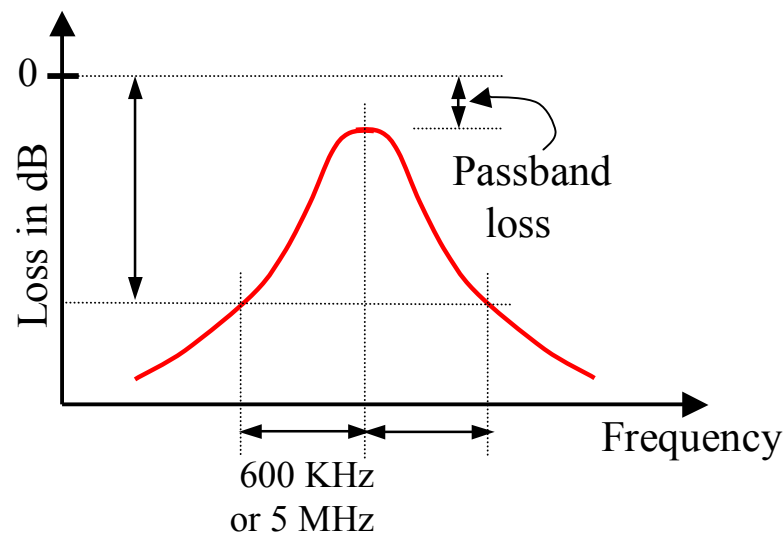
- ❑ CHANGING THE COUPLING TRADES BANDPASS LOSS FOR SELECTIVITY
- ❑ THE Q OF THE COUPLING LOOPS DOES NOT AFFECT THE RESPONSE IF:  $Q > 100$



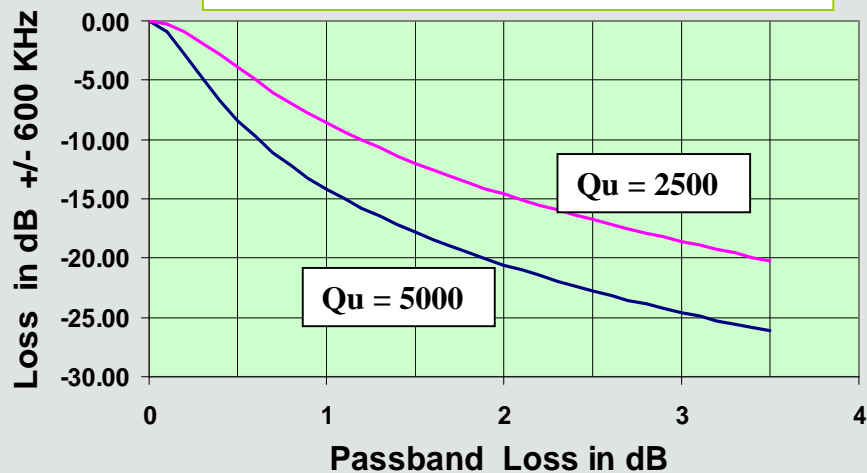


# RESONATOR $Q_u$ , PASSBAND LOSSES AND SELECTIVITY

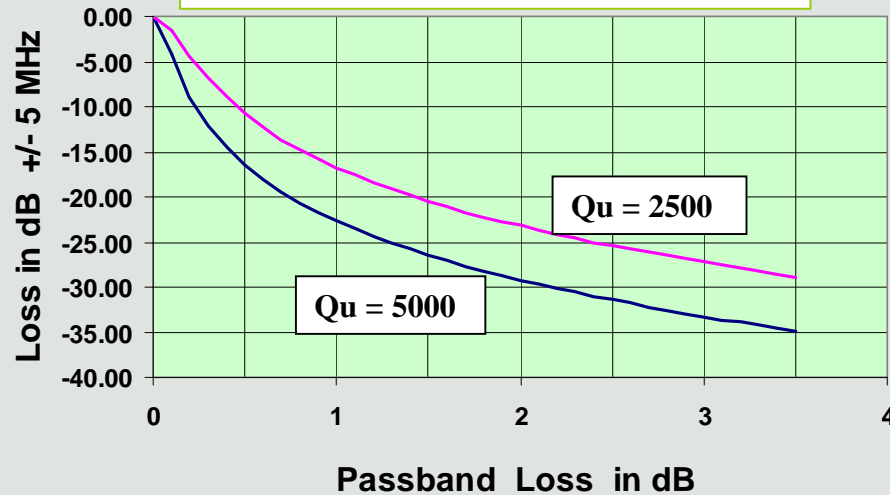
- ❑  $Q_u$  IS THE QUALITY FACTOR OF THE RESONATOR (unloaded Q)
- ❑  $Q_u$  INFLUENCES THE PASSBAND LOSSES AND THE ATTENUATION AWAY FROM THE PASSBAND
- ❑ ONE MAY TRADE PASSBAND LOSS FOR SELECTIVITY AND VICE-VERSA



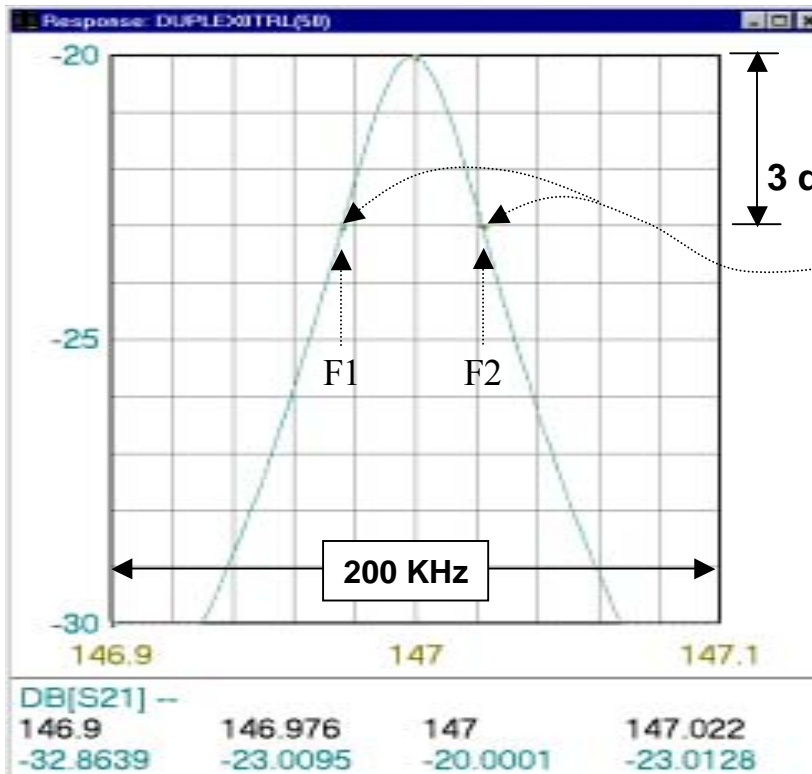
146 MHz Resonator Attenuation  
at +/- 600 KHz offsets



445 MHz Resonator Attenuation  
at +/- 5 MHz offsets



# MEASURING THE Qu FACTOR (Unloaded Q of the cavity)



- Adjust the coupling loops to obtain ~ 20 dB loss in the passband
- Measure and note the frequencies F1 and F2 (in MHz) that give 3 dB attenuation w/r to the peak:
- Calculate the quality factor **Qu**:

$$Q_u = \frac{F_1 + F_2}{2 * (F_2 - F_1)} \quad (\text{Use } F_2 > F_1)$$

**A 6 in. VHF cavity should yield  $Q_u > 4000$ , typically 5000**

Measured values on a 6 in. cavity (notch):  $Q = 4650$  (Davicom Technologies Inc modèle BR-15107)

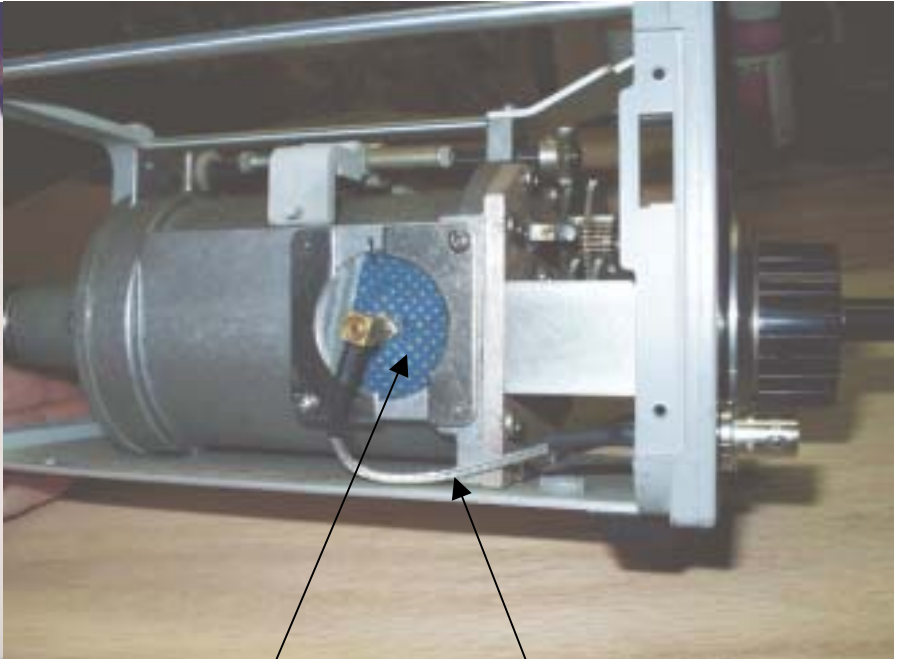
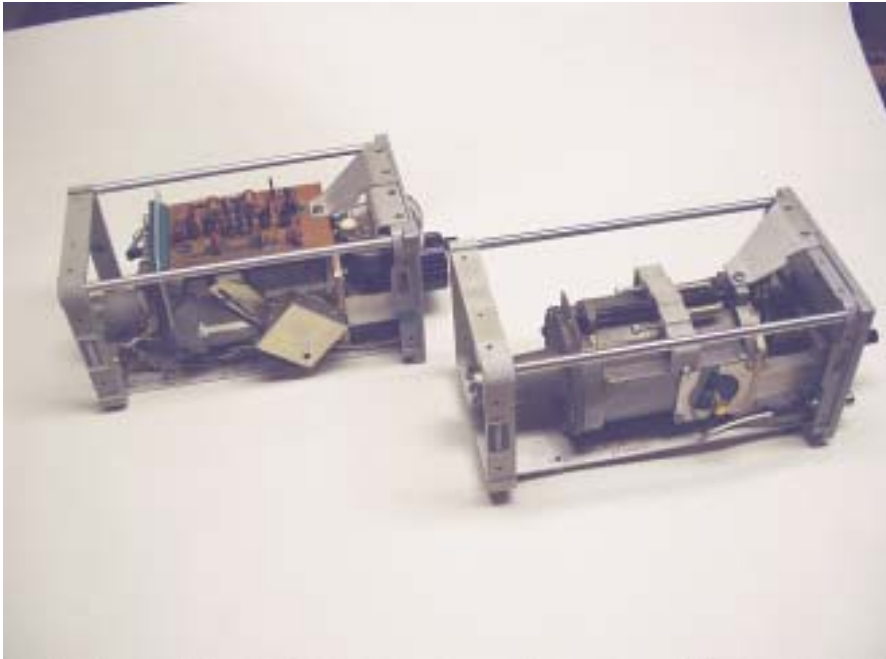
On a 6 in. bandpass cavity:  $Q = 5675$  (Sinclair FP20107\*3)

# A MINIATURE BANDPASS CAVITY FROM HP



- ❑ This is model HP 5253 Plug-in Frequency Converter
- ❑ Easily modified to form a bandpass cavity
- ❑ Covers 50 - 500 MHz frequency range

# A MINIATURE BANDPASS CAVITY FROM HP

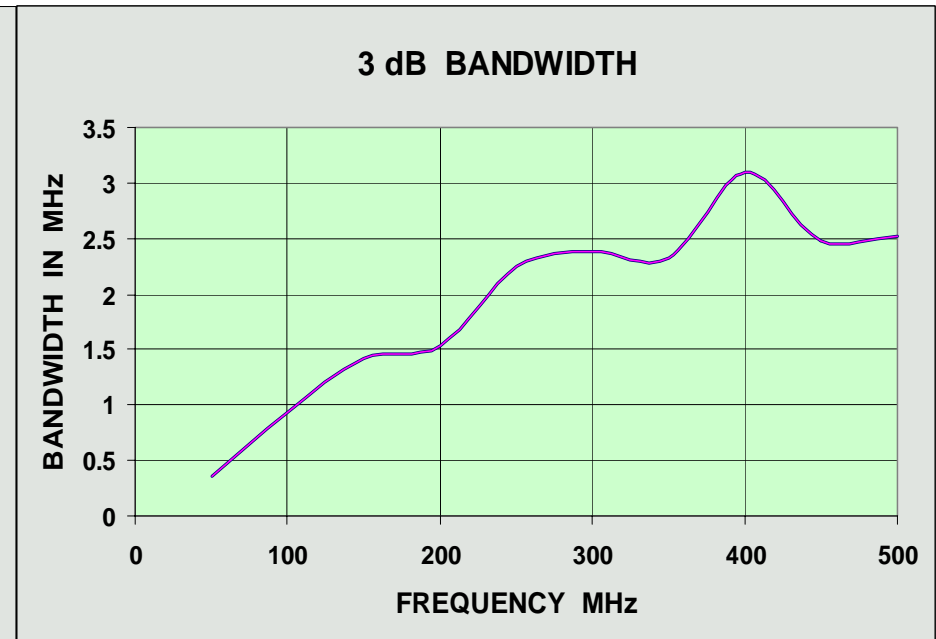
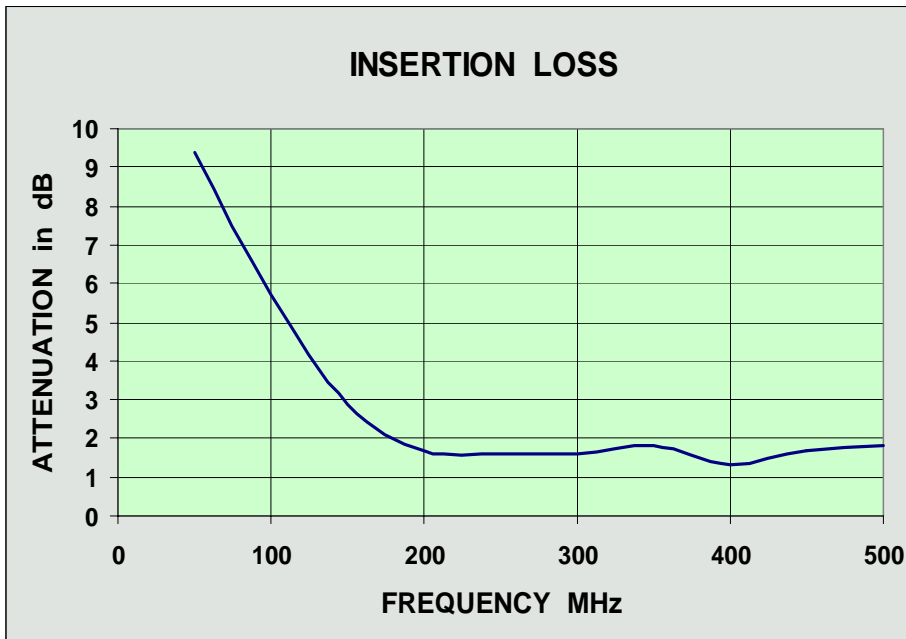


Adding the loop and cable  
(both sides)

# A MINIATURE BANDPASS CAVITY FROM HP

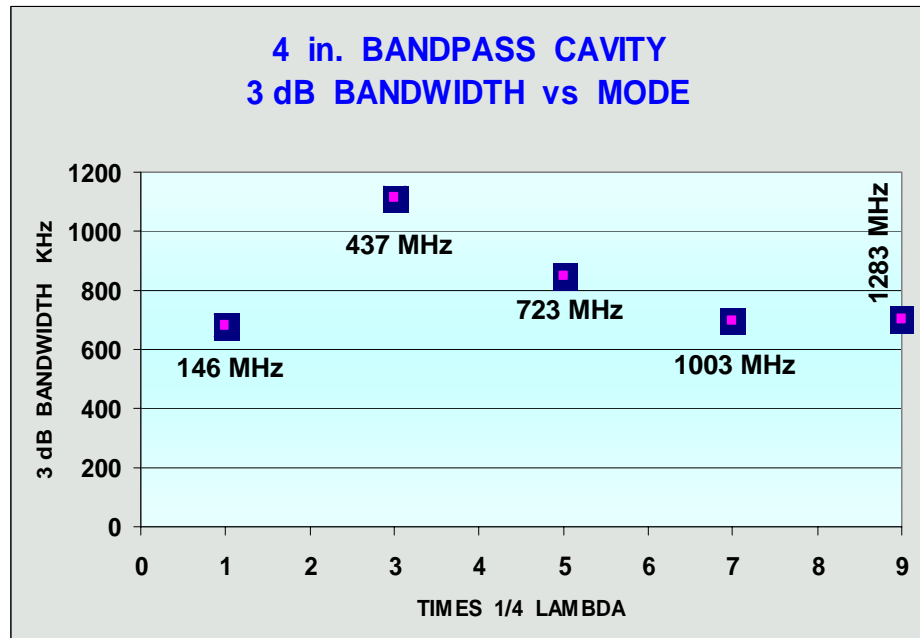
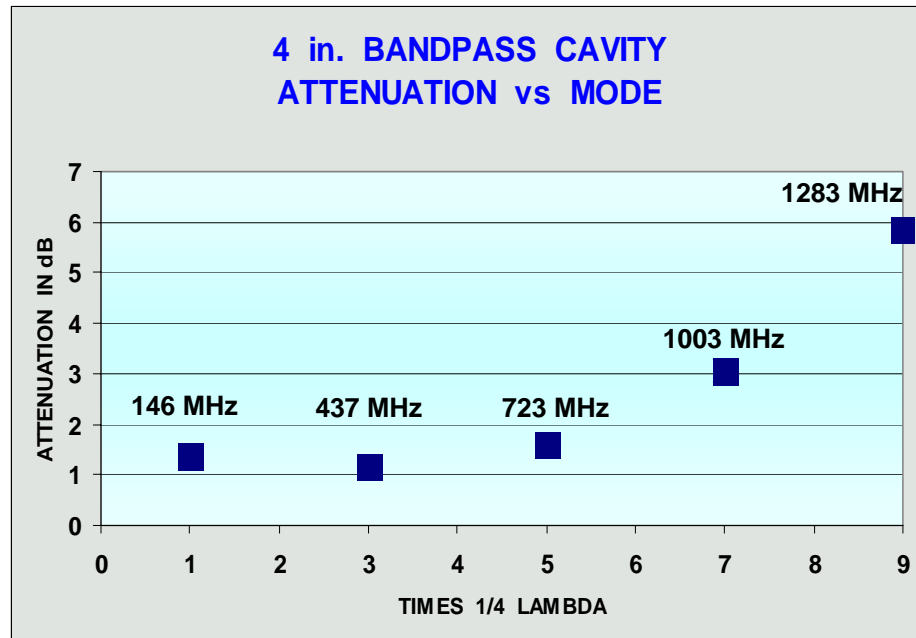
Details of the coupling loop

Note: loops are oriented at right angle of each other



# BANDPASS CAVITIES - OVERTONE OPERATION

- ❑ BANDPASS CAVITIES WILL OPERATE AT ODD MULTIPLES OF THEIR FUNDAMENTAL FREQUENCY
- ❑ OPERATION AT 3X and 5X THE FUNDAMENTAL FREQUENCY PROVIDES LOW LOSSES AND A HIGHER  $Q_u$  FACTOR

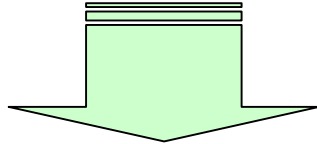


## NOTCH – BANDPASS CAVITIES

- ❑ LO PASS – HI PASS FILTERS

- ❑ BANDPASS CAVITIES

- ➔ ❑ NOTCH – BANDPASS CAVITIES



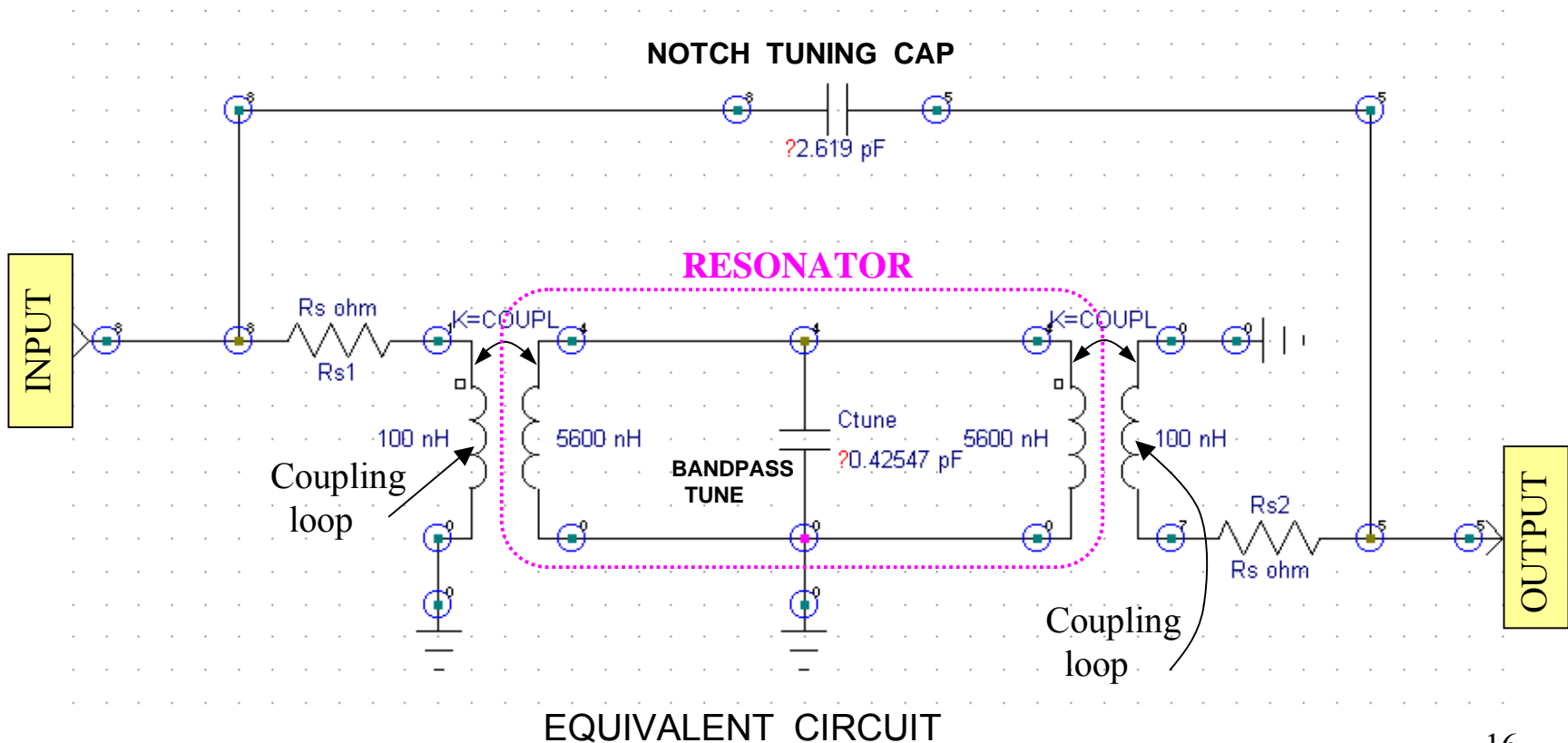
- ➔ ❑ TWO LOOP CAVITIES (modified bandpass)

- ❑ SERIES RESONANT LOOP

- ❑ PARALLEL RESONANT LOOP (Q circuit)

## TWO LOOP CAVITIES (modified bandpass)

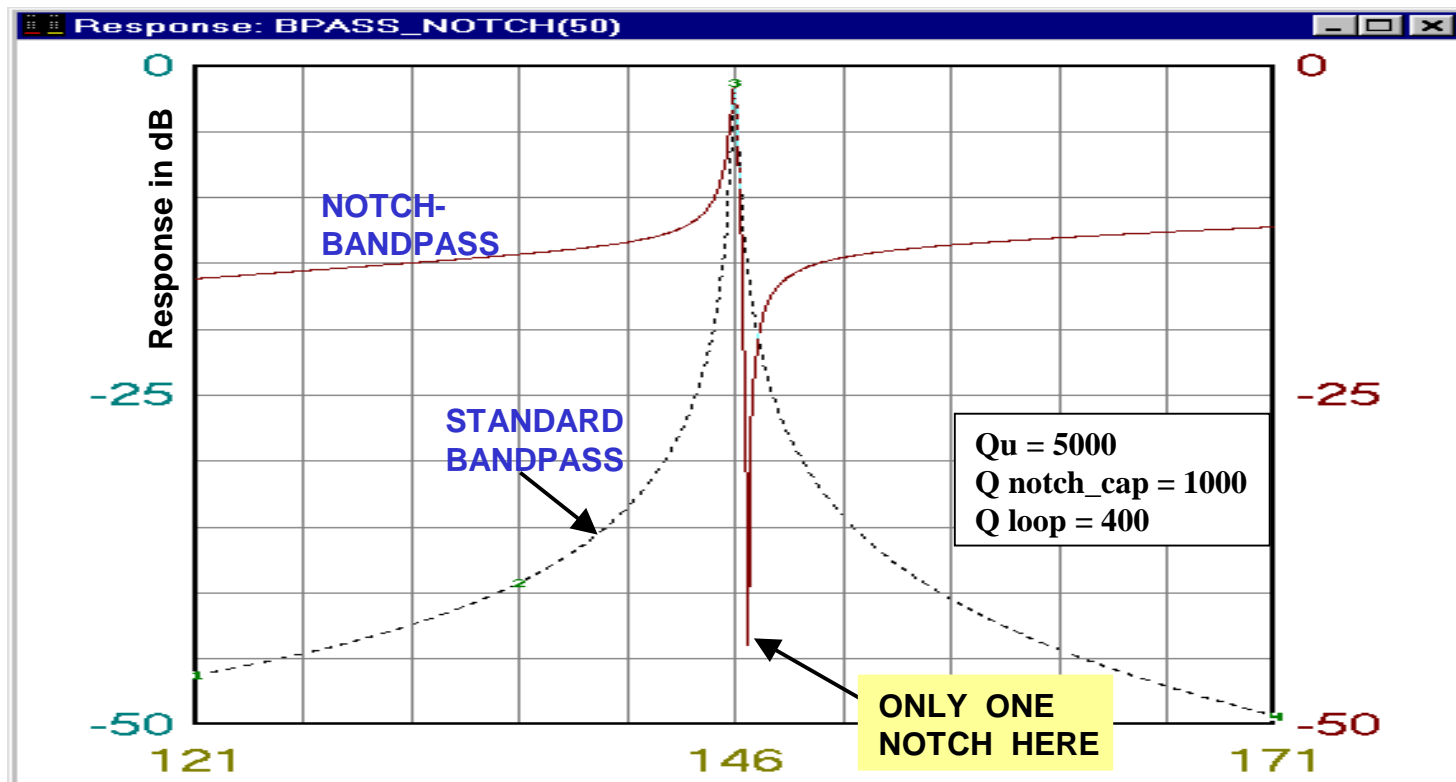
- ❑ A LOW VALUE CAPACITOR IS ADDED BETWEEN INPUT AND OUTPUT
- ❑ GENERATES A TRANSMISSION NOTCH ABOVE BANDPASS
- ❑ AN INDUCTOR WILL SET THE NOTCH BELOW THE BANDPASS





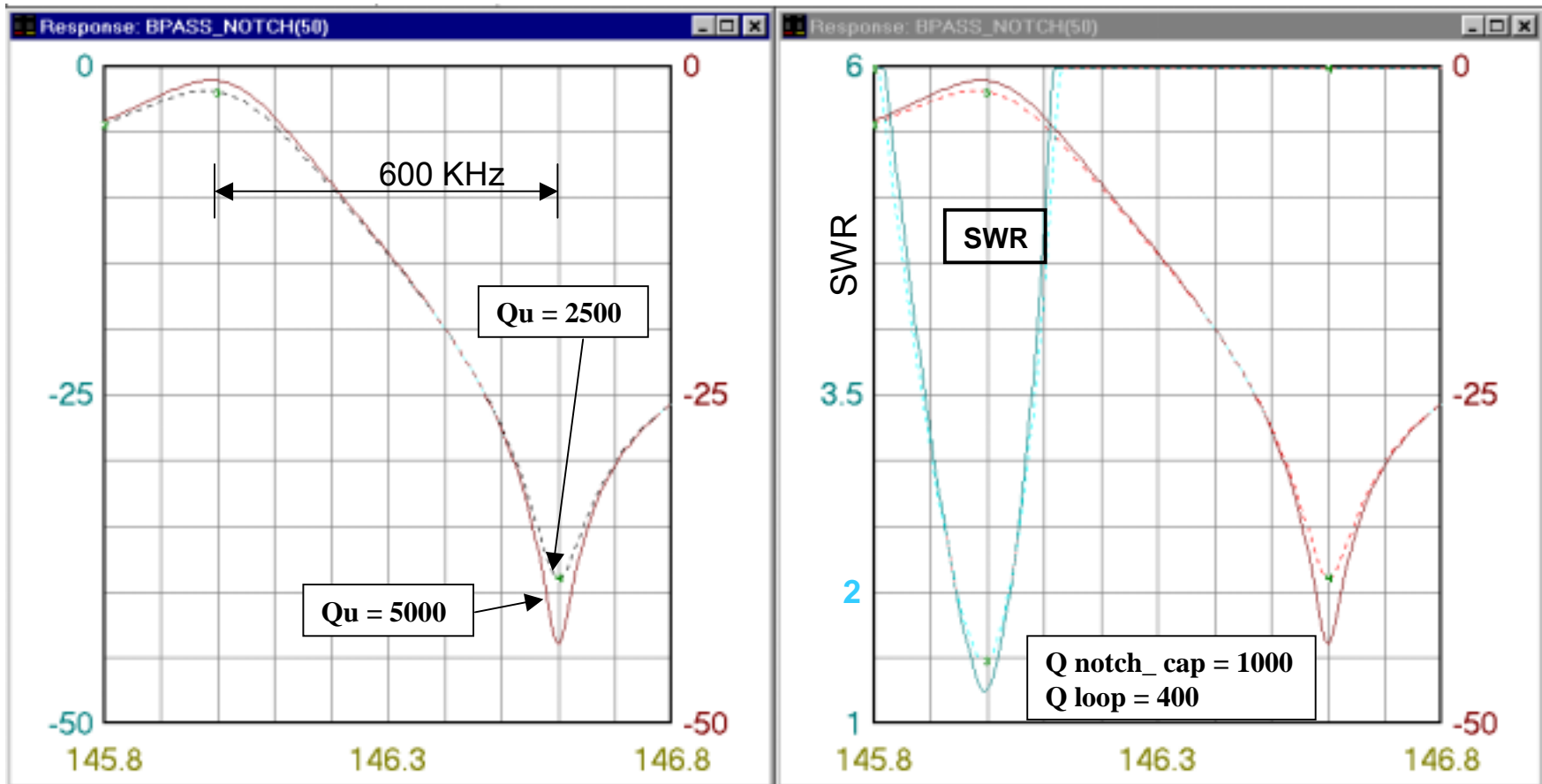
## TWO LOOP CAVITIES (modified bandpass)

- ❑ SERIES CAPACITOR BETWEEN INPUT AND OUTPUT ( $\sim 3$  pF) GIVES THE DESIRED NOTCH-BANDPASS CHARACTERISTIC – ALLOWS NOTCH TUNING
- ❑ SERIES CAPACITOR TUNING SENSITIVITY:  $\sim -20\%$  PER 100 KHz (146 MHz) (REDUCING C MOVES THE NOTCH UP IN FREQUENCY)
- ❑ BANDPASS LOSS  $\sim$  UNCHANGED – COMPARED TO STANDARD BANDPASS



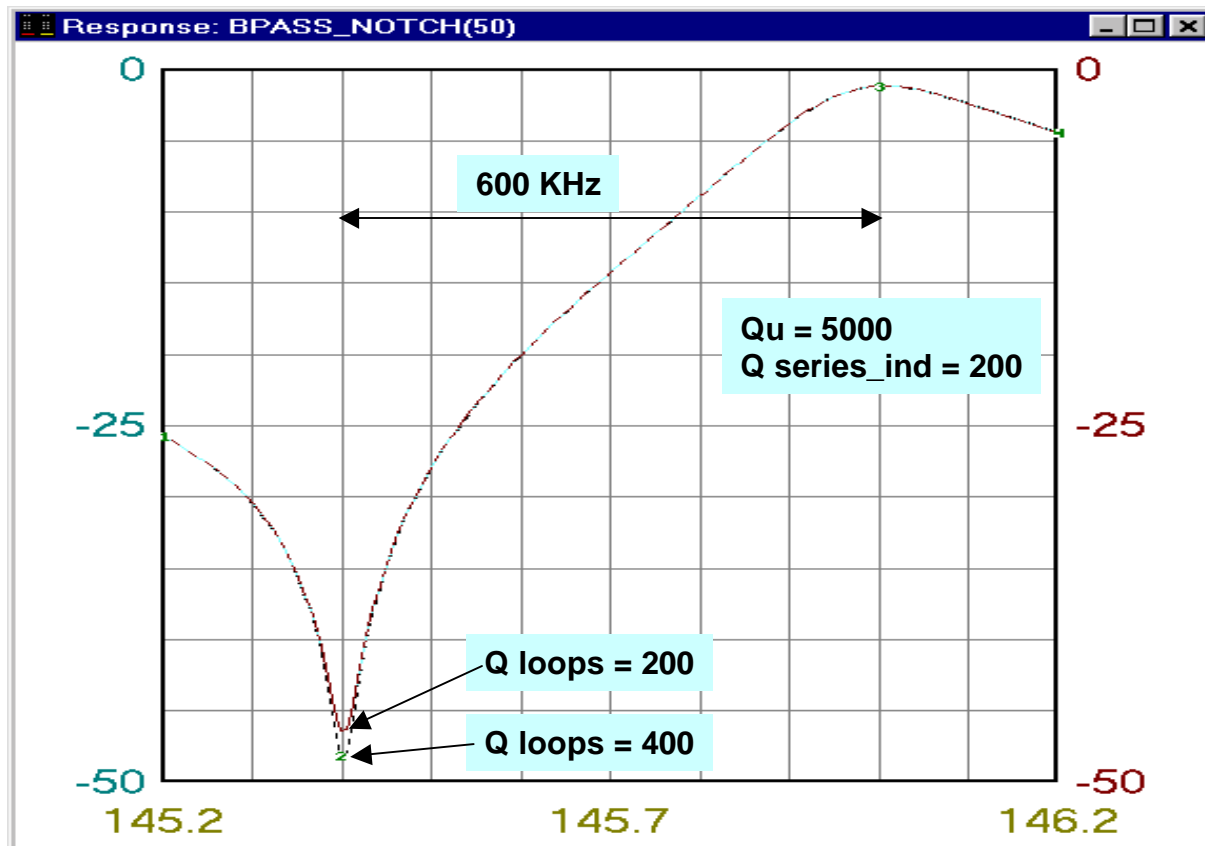
## TWO LOOP CAVITIES (modified bandpass)

- ❑ REDUCING  $Q_u$  FROM 5000 TO 2500 REDUCES THE NOTCH BY ~ 5 dB AND ADDS ~ 1 dB LOSS IN THE BANDPASS
- ❑ THE BANDPASS CENTER HAS LOWEST SWR - ALWAYS



## TWO LOOP CAVITIES (modified bandpass)

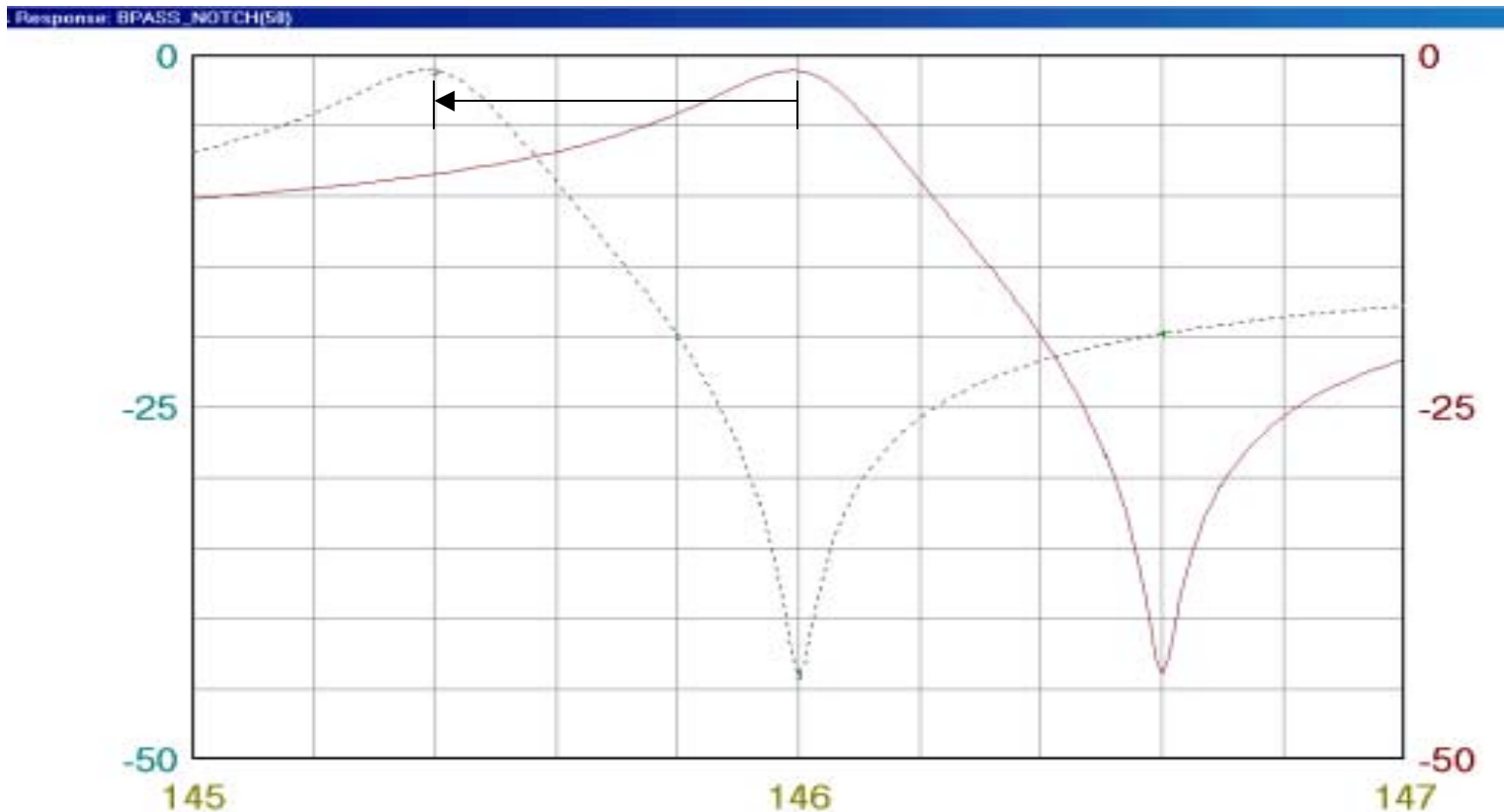
- ❑ SETTING THE **NOTCH BELOW THE BANDPASS** REQUIRES REPLACING THE SERIES CAP BY A SERIES INDUCTOR (~ 400 nH)
- ❑ REDUCING THE Q FACTOR OF THE LOOPS FROM 400 TO 200 DEGRADES THE NOTCH DEPTH BY ~ 3 dB



SETTING THE NOTCH BELOW THE BANDPASS


## TWO LOOP CAVITIES (modified bandpass)

- ❑ INCREASING THE RESONATOR LENGTH MOVES THE BANDPASS FREQUENCY DOWN
- ❑ SHIFTING THE BANDPASS FREQUENCY DOWN ALSO SHIFTS THE NOTCH FREQUENCY BY APPROXIMATELY THE SAME AMOUNT



MOVING THE BANDPASS FREQUENCY DOWN

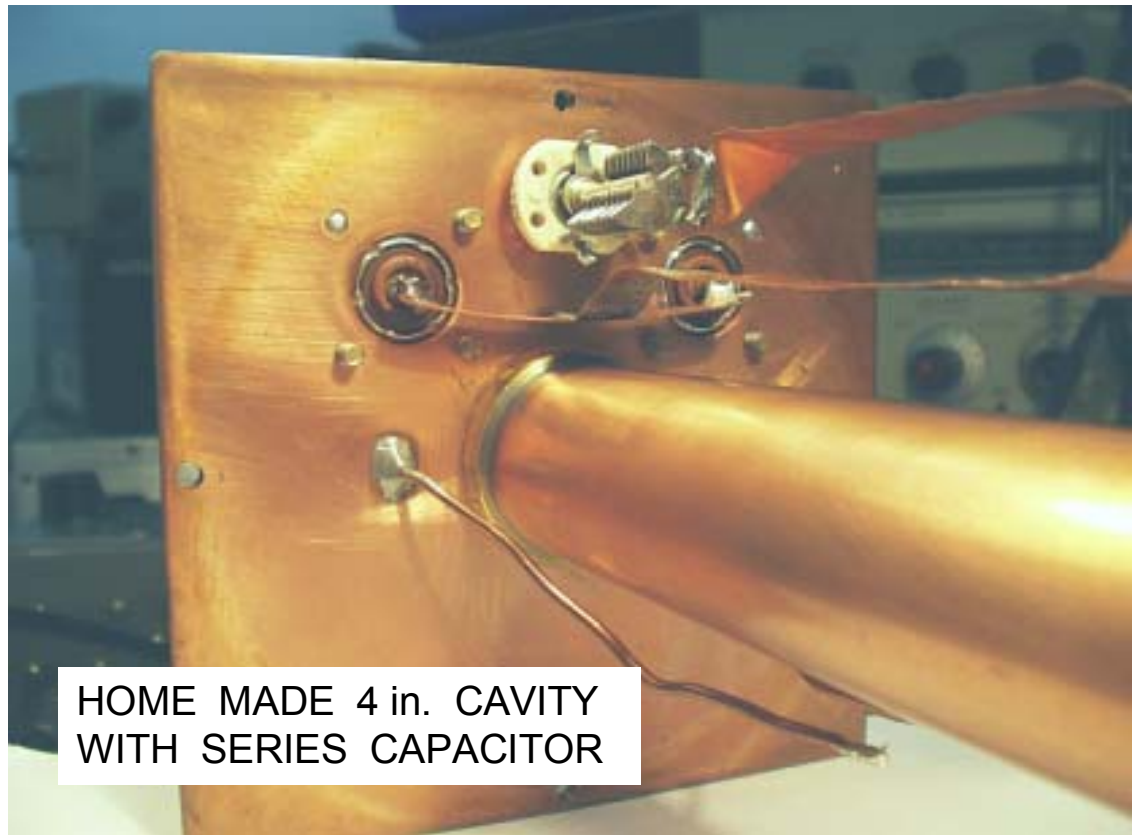
## NOTCH – BANDPASS SERIES RESONANT LOOP CAVITIES

- TWO LOOP CAVITY (modified bandpass)
-   SERIES RESONANT LOOP
- PARALLEL RESONANT LOOP (Q circuit)

## SERIES RESONANT LOOP

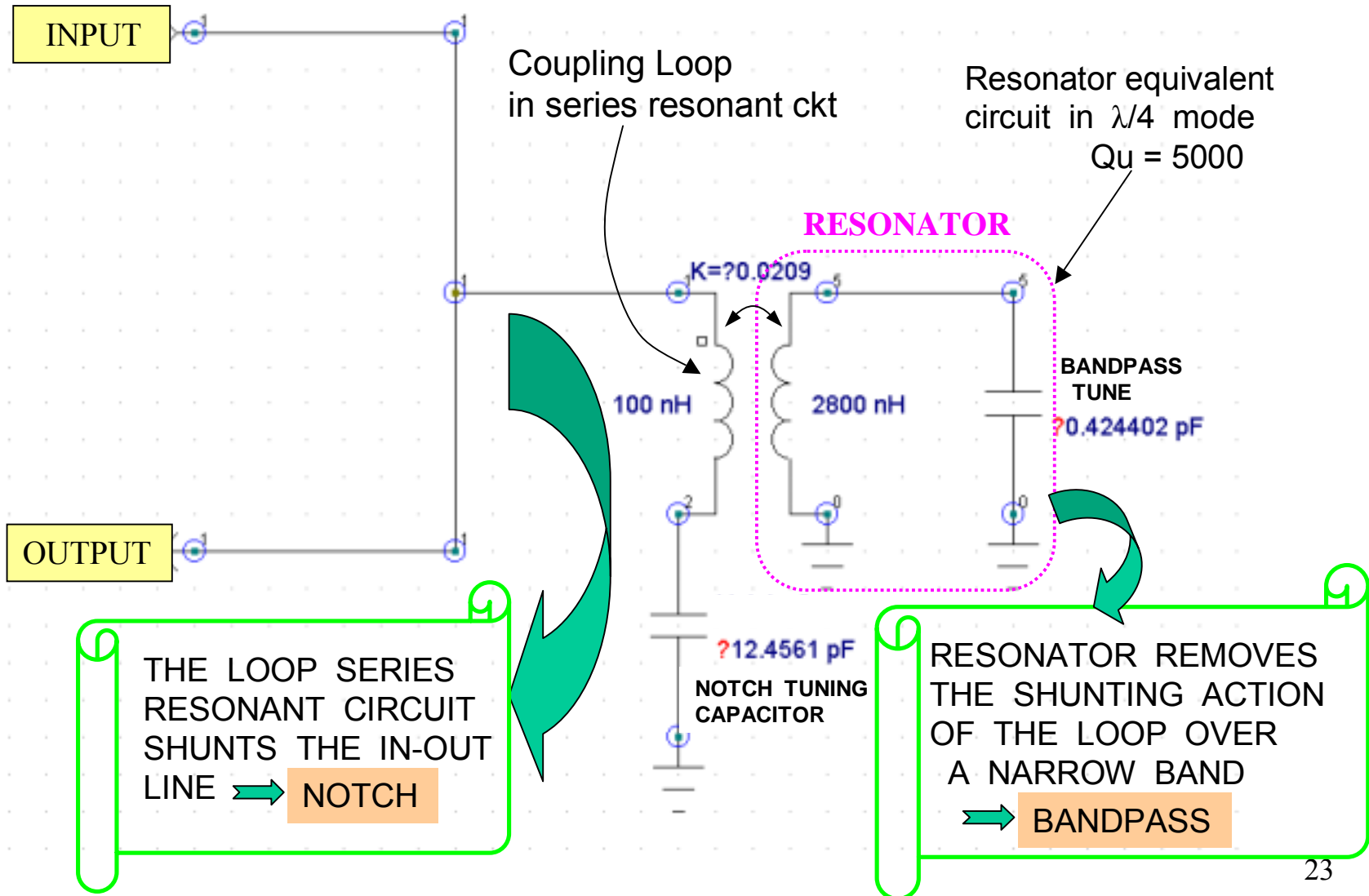
- ❑ ONLY ONE LOOP IS USED
- ❑ A SERIES CAPACITOR ADJUSTS THE NOTCH FREQUENCY ABOVE AND BELOW THE BANDPASS

A SINGLE CONNECTOR WITH AN EXTERNAL TEE WILL WORK AS WELL



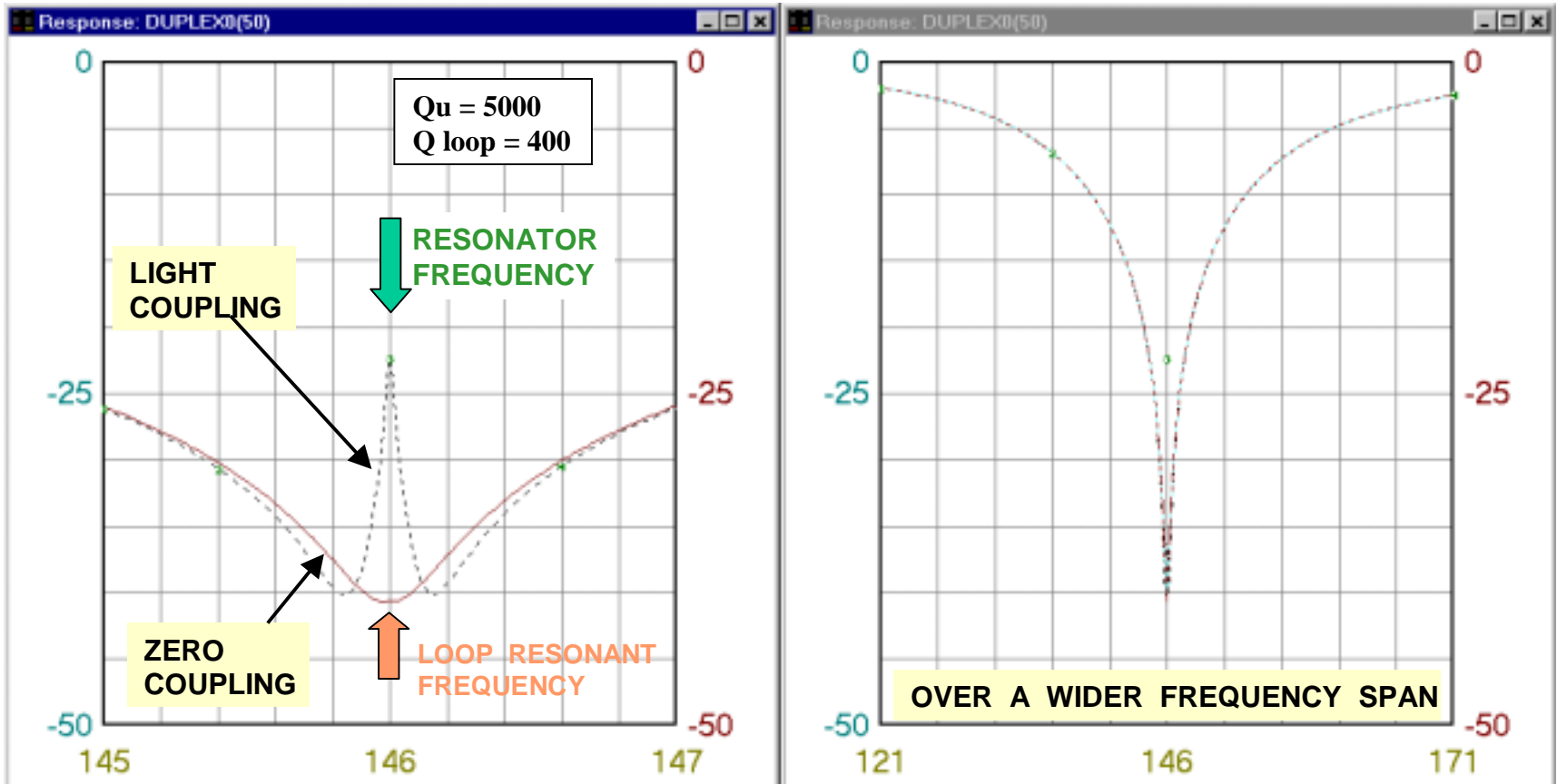
# SERIES RESONANT LOOP

GIVES NOTCH – BANDPASS RESPONSE



# SERIES RESONANT LOOP

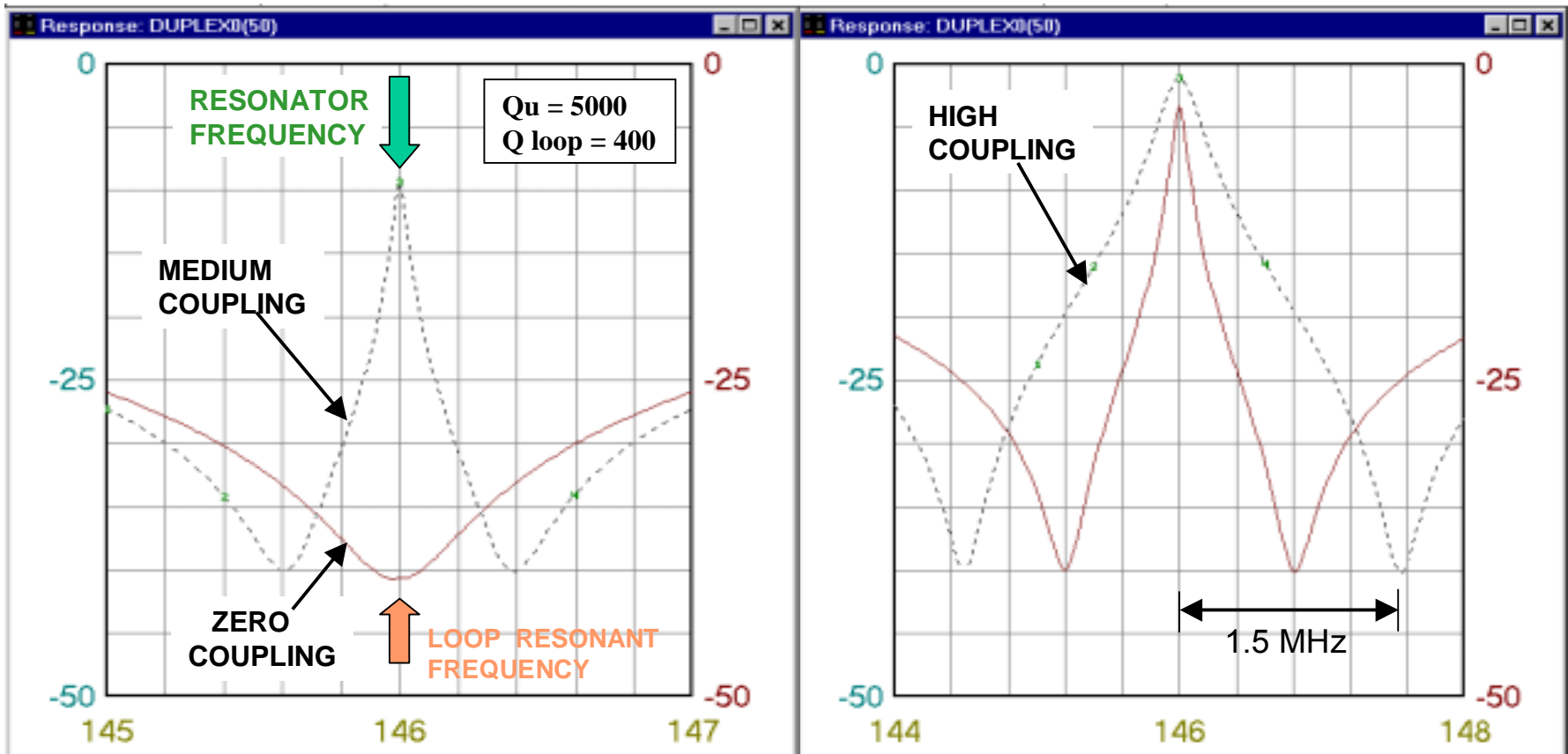
- ❑ THE COUPLING LOOP IS INITIALLY UNCOUPLED FROM THE RESONATOR
- ❑ SERIES CIRCUIT GIVES MAXIMUM ATTENUATION AT SERIES RESONANCE
- ❑ THE RESONATOR IS TUNED AT THE SAME FREQUENCY
- ❑ NOTCH DEPTH IS A FUNCTION OF THE Q OF THE LOOP





# SERIES RESONANT LOOP

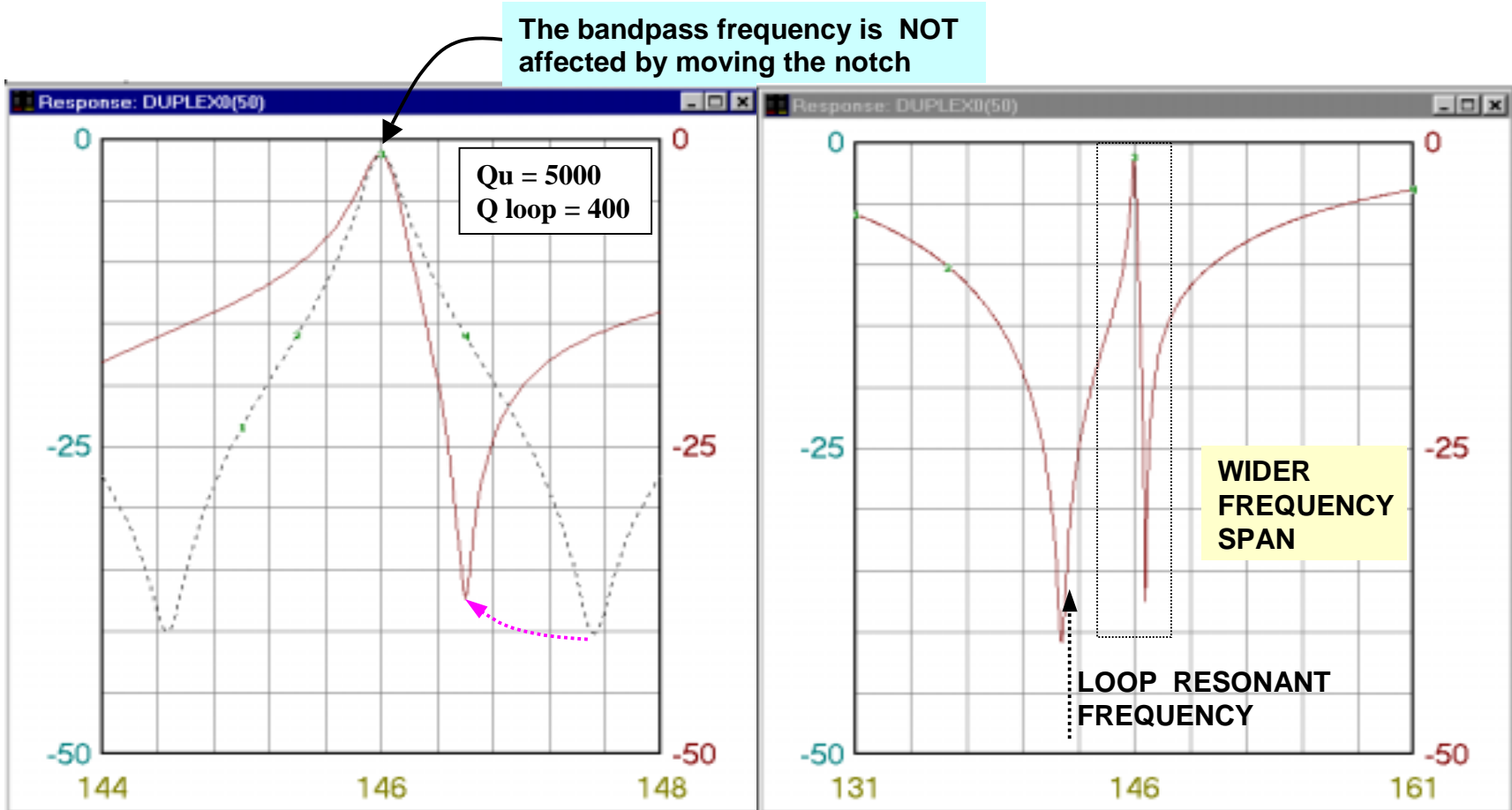
- ❑ INCREASING THE COUPLING SPREADS THE TWO NOTCHES APART AND...
- ❑ DECREASES THE INSERTION LOSS AT THE BANDPASS FREQUENCY
- ❑ FOR 1 dB LOSS THE NOTCHES ARE AT +/- 1.5 MHz – NEED TO SHIFT



EFFECT OF CHANGING THE LOOP COUPLING

# SERIES RESONANT LOOP

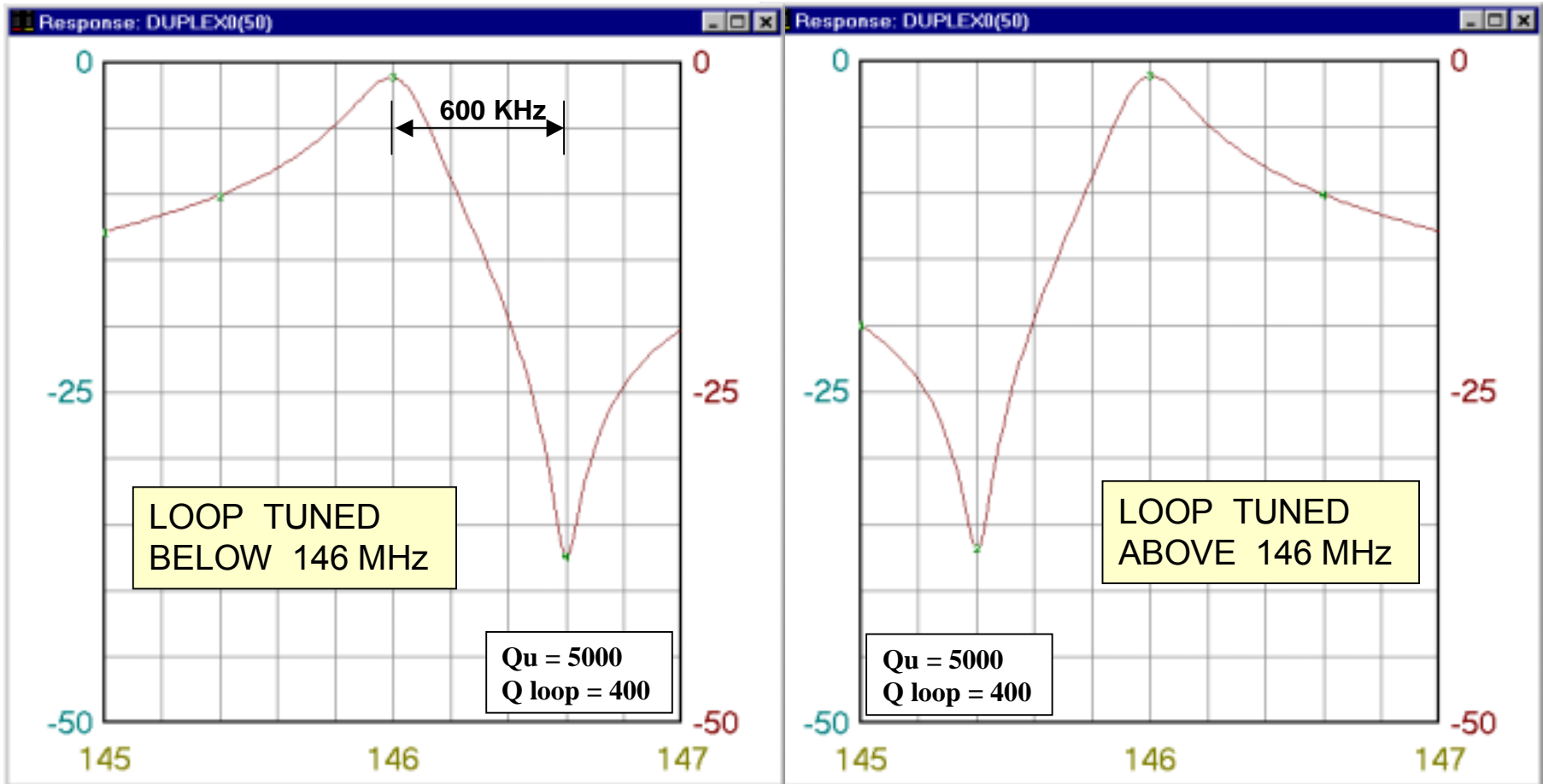
- ❑ THE UPPER NOTCH FREQUENCY IS SHIFTED DOWN BY LOWERING THE LOOP RESONANT FREQUENCY (BROWN CURVES)
- ❑ THE DEPTH OF THE UPPER NOTCH SUFFERS



SHIFTING DOWN THE NOTCH FREQUENCY

# SERIES RESONANT LOOP

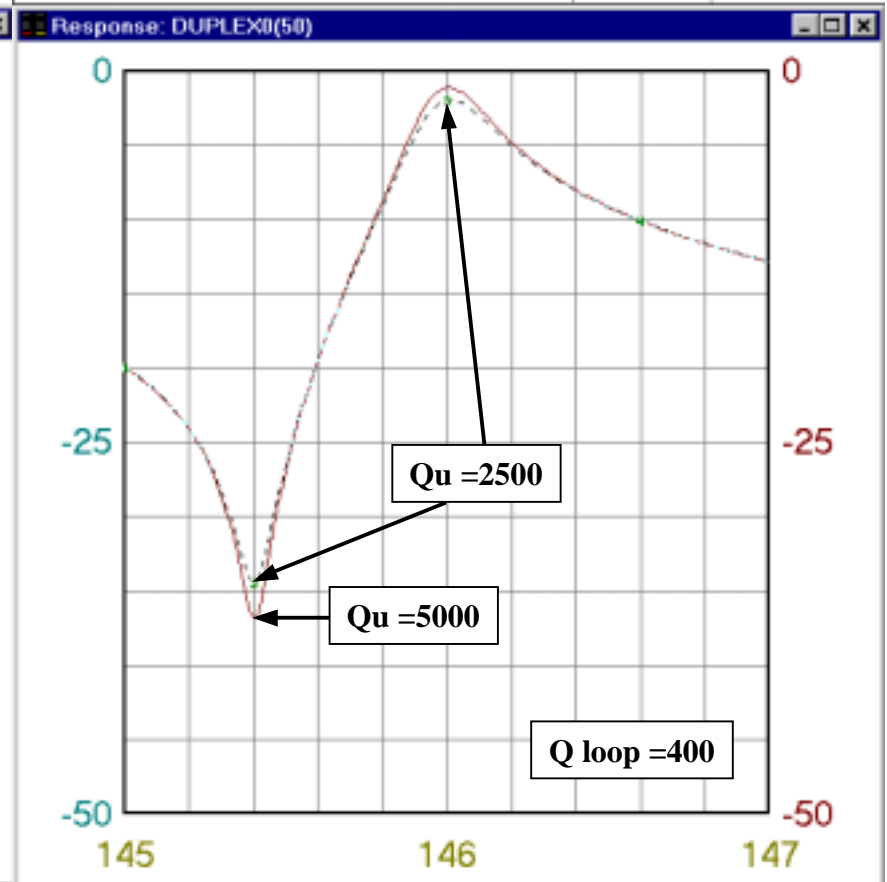
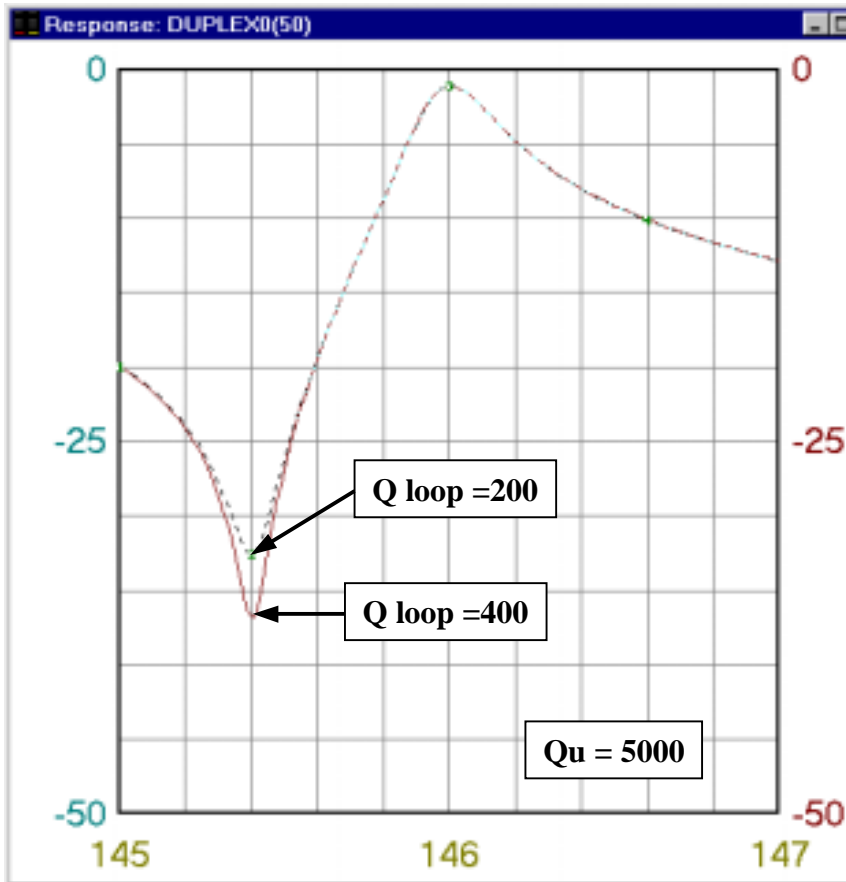
- ❑ TUNING THE LOOP BELOW AND ABOVE THE BANDPASS FREQUENCY WILL SET THE NOTCH  $\pm 600$  KHz



# SERIES RESONANT LOOP

- THE Q OF THE LOOP SETS THE NOTCH DEPTH

- THE Q OF THE CAVITY ( $Q_u$ ) AFFECTS BOTH THE BANDPASS LOSS AND THE NOTCH DEPTH

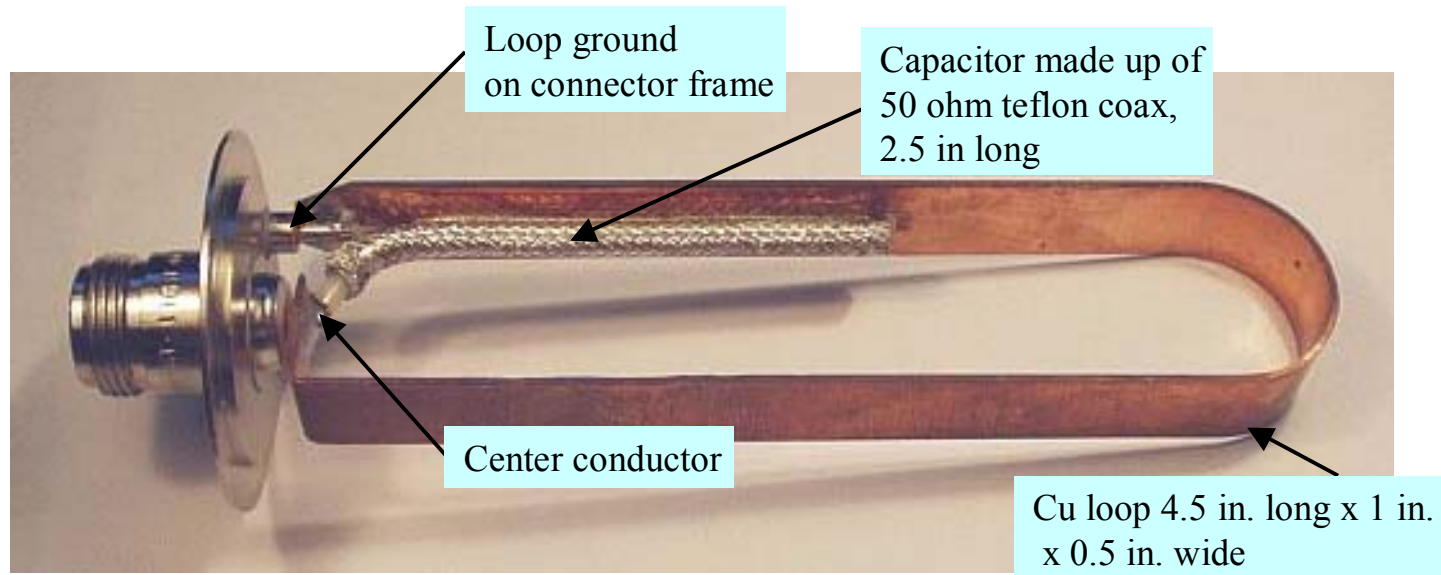


## NOTCH – BANDPASS MODE PARALLEL RESONANT LOOP CAVITIES

- ❑ TWO LOOP CAVITY (modified bandpass)
- ❑ SERIES RESONANT LOOP
- ➡ ❑ PARALLEL RESONANT LOOP (Q circuit)

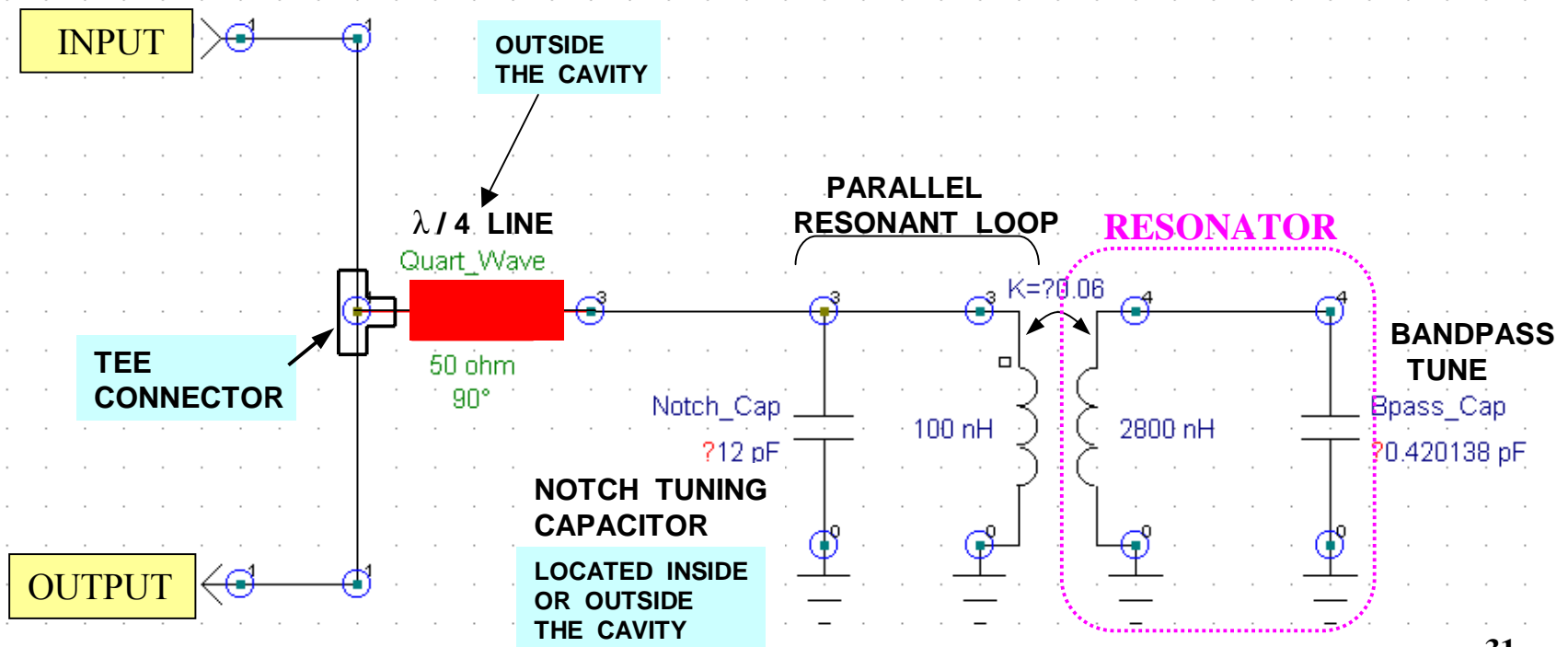
## PARALLEL RESONANT LOOP (Q circuit)

- ❑ EXAMPLE OF A PARALLEL RESONANT LOOP
- ❑ HERE THE CAPACITOR IS MADE WITH A SHORT LENGTH OF COAX



## PARALLEL RESONANT LOOP (Q circuit)

- ❑ A QUARTER WAVELENGTH LINE TRANSFORMS THE LOOP PARALLEL CIRCUIT INTO A SERIES CIRCUIT – EFFECTIVELY
- ❑ OPERATION IS SIMILAR TO THE SERIES RESONANT LOOP
- ❑ TWO NOTCHES ARE ALWAYS PRESENT WITH THIS CONFIGURATION



## NOTCH CAVITIES

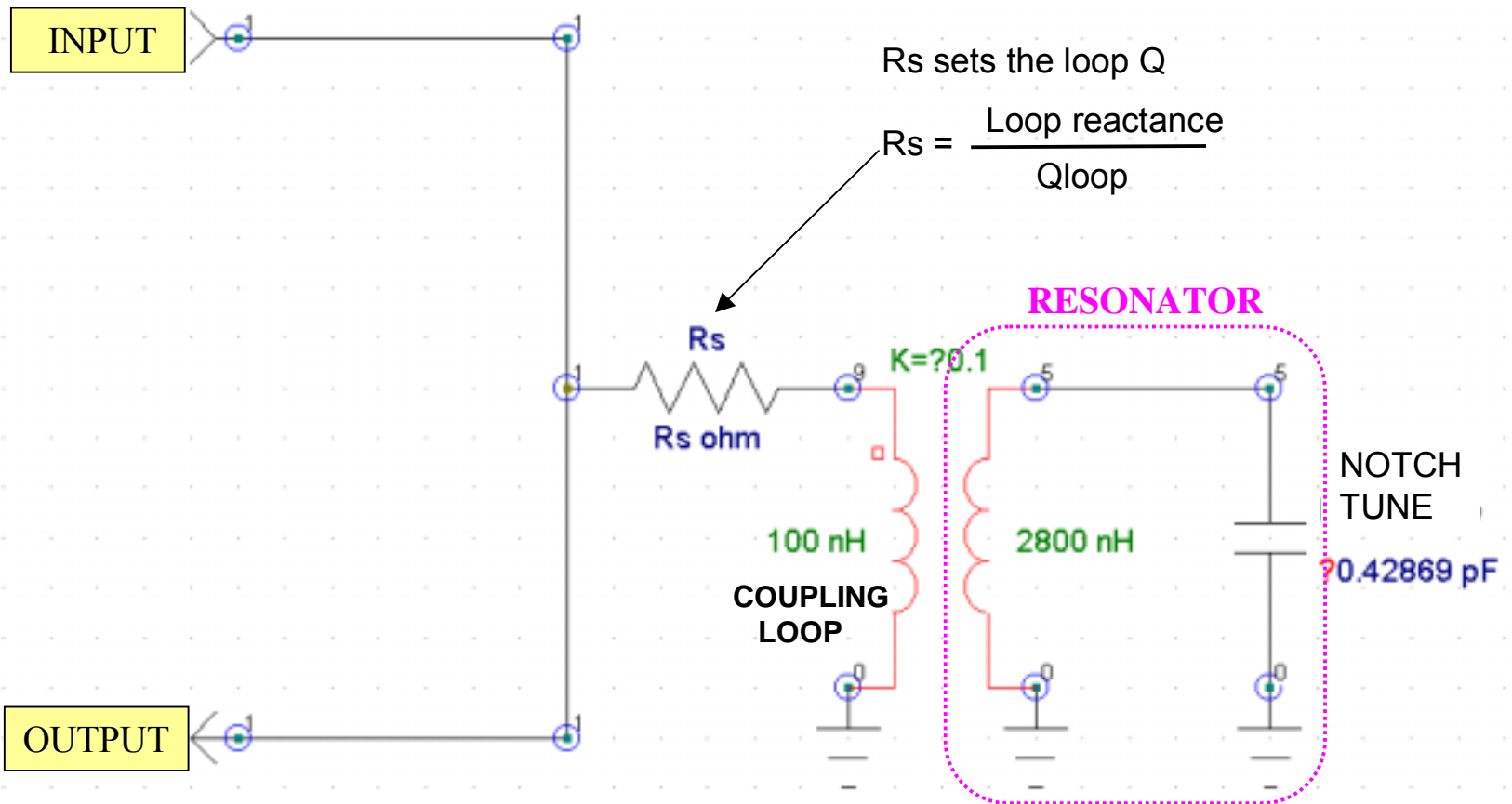
  CAVITY NOTCHERS

HELIAX NOTCHERS



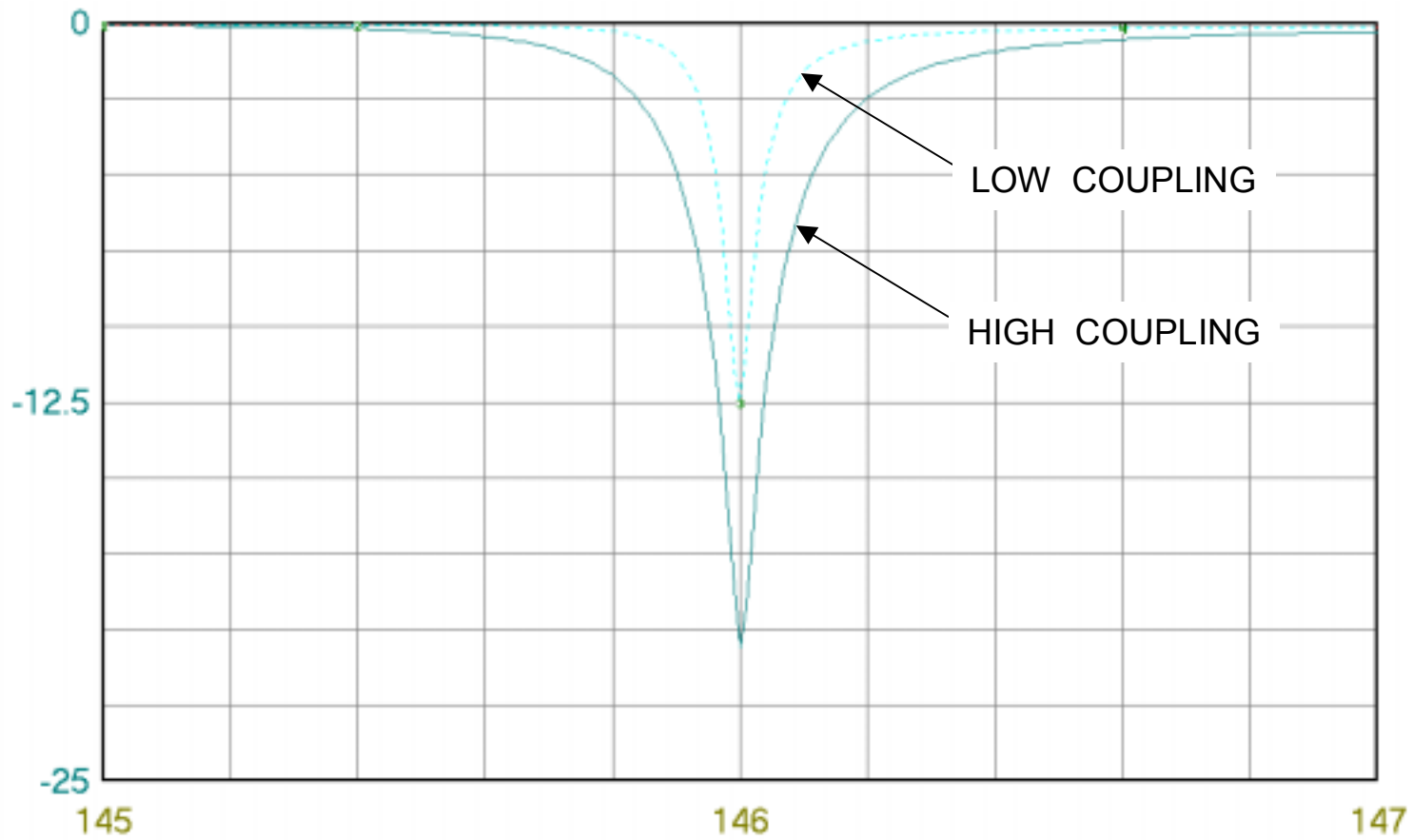
# CAVITY NOTCHER for 146 MHz

## EQUIVALENT CIRCUIT



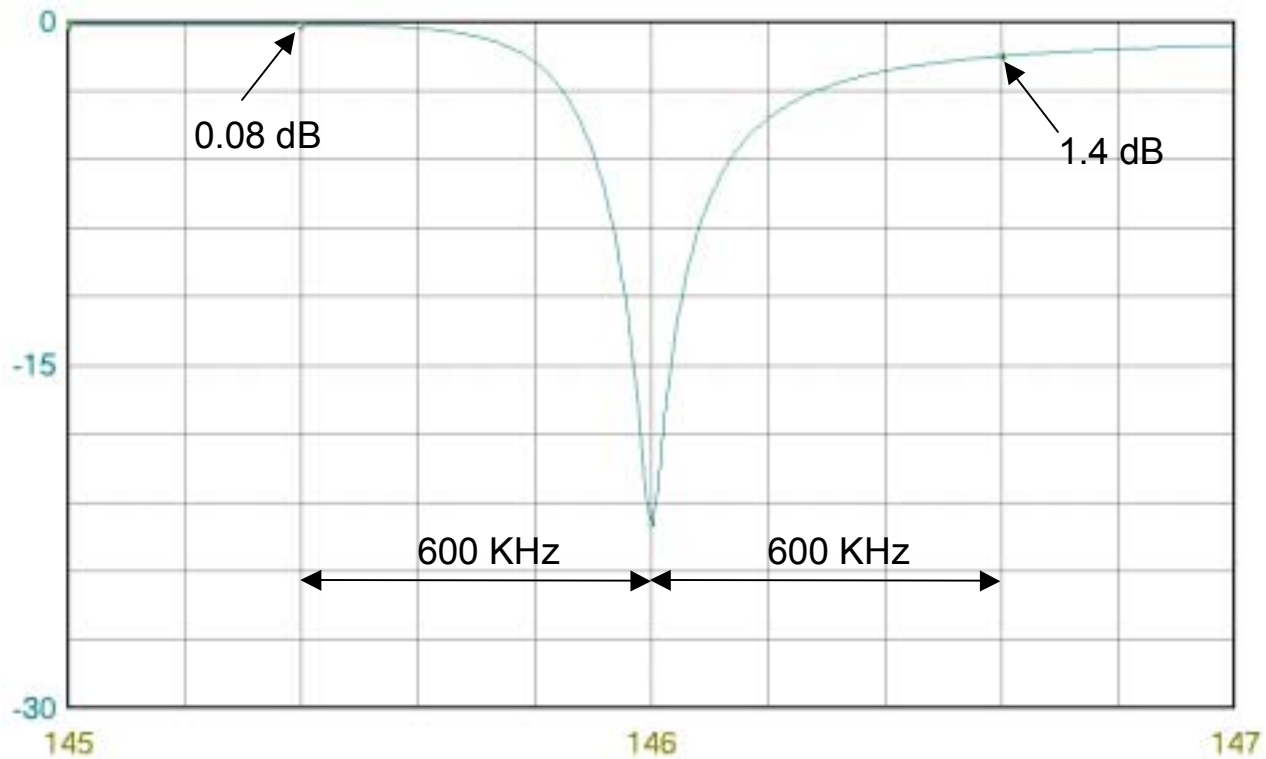
# CAVITY NOTCHER FREQUENCY RESPONSE

- ❑ VARYING THE LOOP COUPLING AFFECTS THE NOTCH DEPTH AND
- ❑ DETUNES THE NOTCH FREQUENCY SOMEWHAT



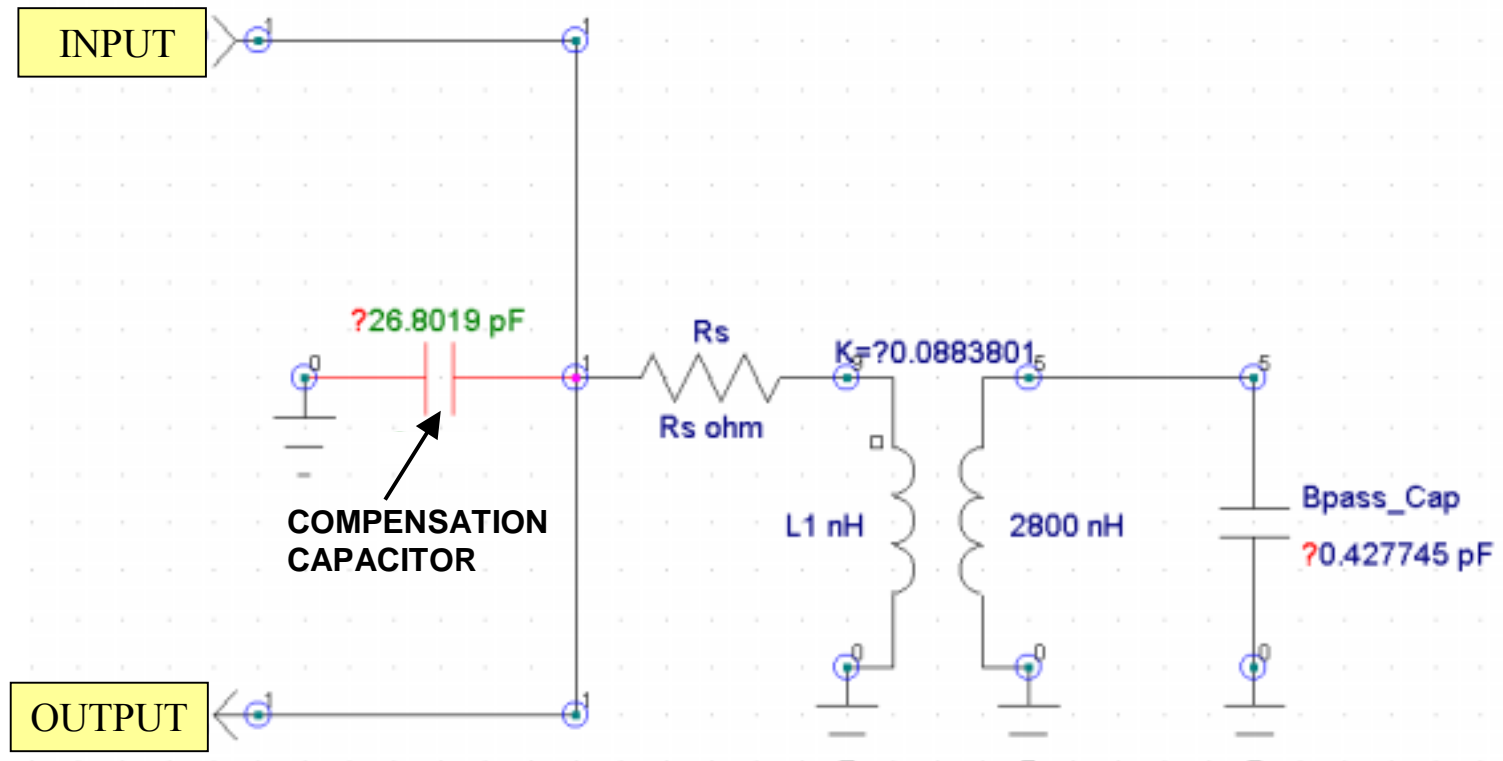
# CAVITY NOTCHER FREQUENCY RESPONSE

- ❑ RESPONSE NOT SYMETRICAL AT +/- 600 KHz
- ❑ HIGH SIDE HAS A LOT MORE ATTENUATION AT + 600KHz



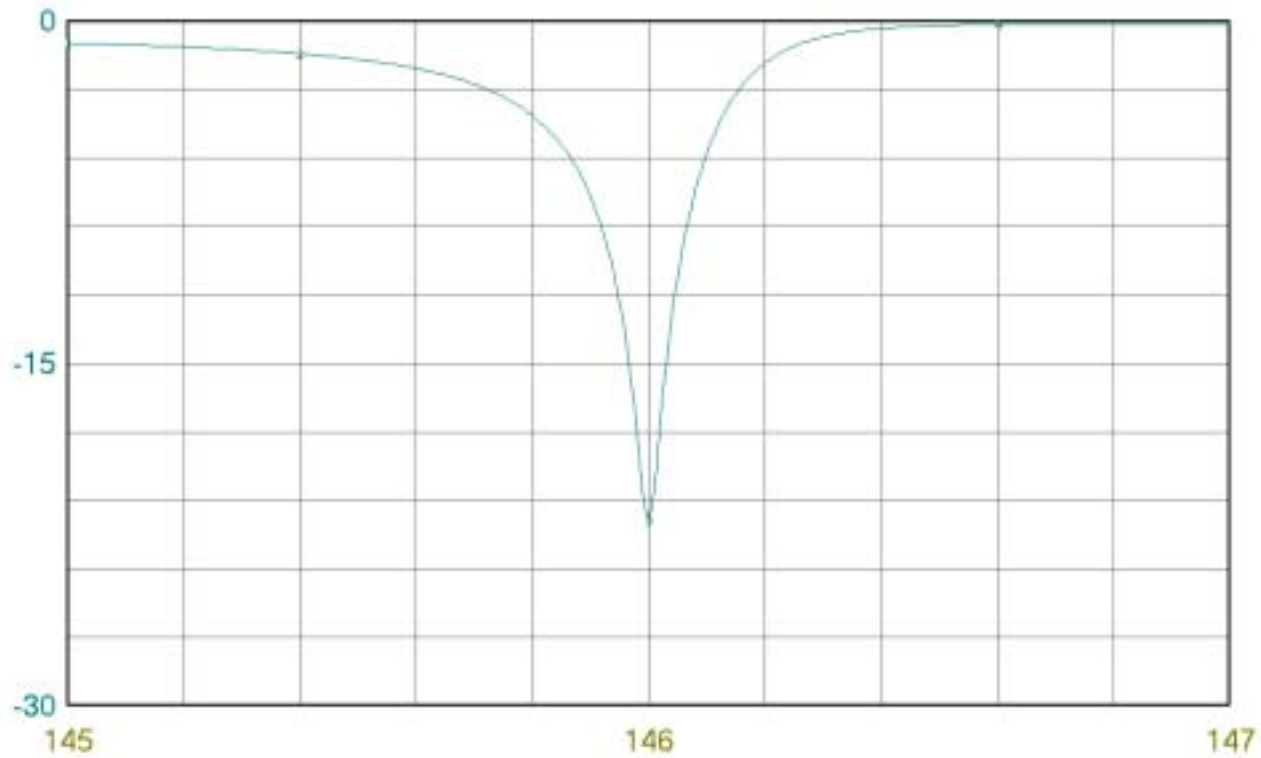
# CAVITY NOTCHER WITH COMPENSATION CAPACITOR

- ❑ ADDING A COMPENSATION CAPACITOR DECREASES THE LOSSES ON THE UPPER SIDE
- ❑ THE COMPENSATION CAPACITOR HAS AN OPTIMUM VALUE FOR A GIVEN SPLIT
- ❑ ITS Q FACTOR IS NOT CRITICAL - AN OPEN COAX STUB MAY BE USED



## CAVITY NOTCHER WITH COMPENSATION CAPACITOR

- ❑ CONSIDERABLY REDUCED HIGH SIDE INSERTION LOSS
- ❑ LOW SIDE NOW HAS THE HIGH INSERTION LOSS



## CAVITY NOTCHERS - GENERAL

- ❑ OBTAINING THE DEEPEST NOTCH REQUIRES:
  - INCREASING THE LOOP COUPLING
  - DECREASING THE LOOP INDUCTANCE
- ❑ THESE TWO REQUIREMENTS ARE CONTRADICTORY SINCE
  - A LOW INDUCTANCE LOOP WILL HAVE LESS COUPLING AND VICE VERSA
- ❑ IT MAY BE DIFFICULT TO GET 30 dB REJECTION ON A 6 in. CAVITY
- ❑ THE LOW SIDE MAY HAVE TO BE COMPENSATED WITH AN INDUCTOR
  - TO ACHIEVE MINIMUM LOSSES (OR A SHORTED STUB)
- ❑ THE Q FACTOR OF THE LOOPS IS NOT CRITICAL, AS LONG AS  $Q > 100$  OR SO
- ❑ THE NOTCH - BANDPASS MODE MAKES A MORE EFFICIENT USE OF THE CAVITY.
  - NOTCH DEPTHS BETTER THAN 35 dB ARE EASILY OBTAINED WITH A 6 in. CAVITY

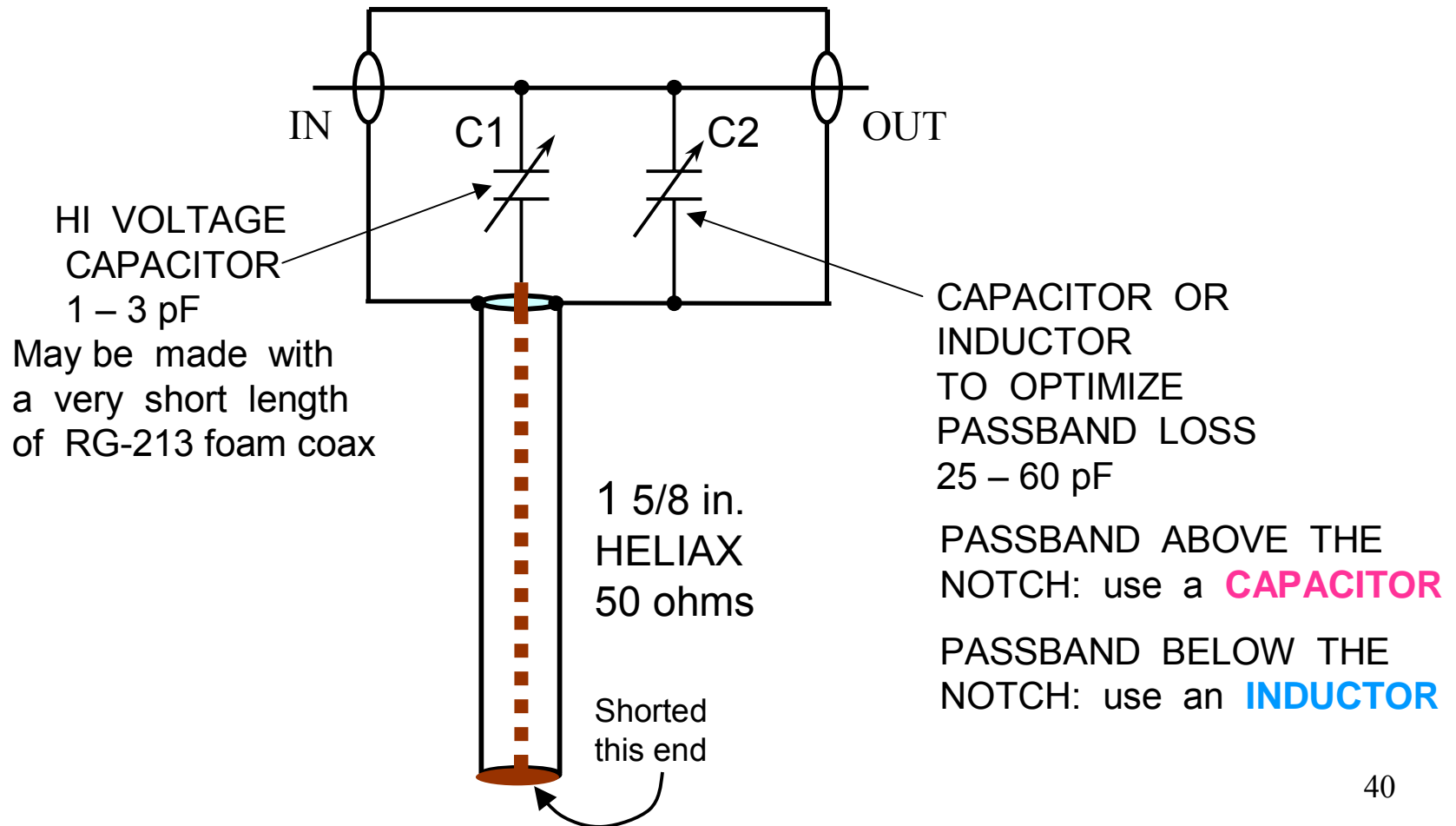
## NOTCH CAVITIES

- CAVITY NOTCHERS

-  □ HELIAX NOTCHERS

# HELIAX NOTCHER for 146 MHz

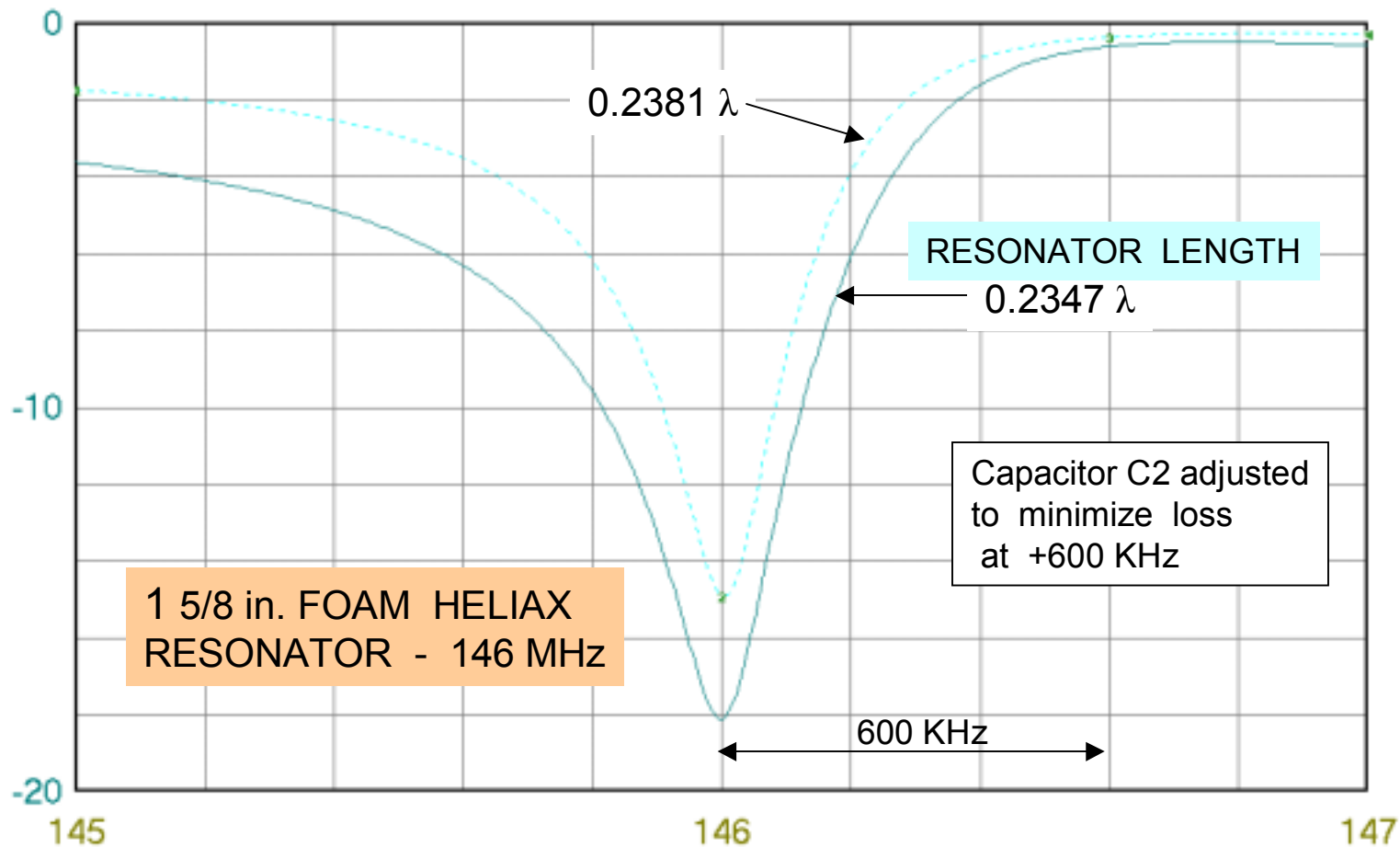
- ❑ USES AN INDUCTIVE SHORTED STUB See ref. 3 and 4
- ❑ THE STUB EXHIBITS SERIES RESONANCE AT THE NOTCH FREQUENCY





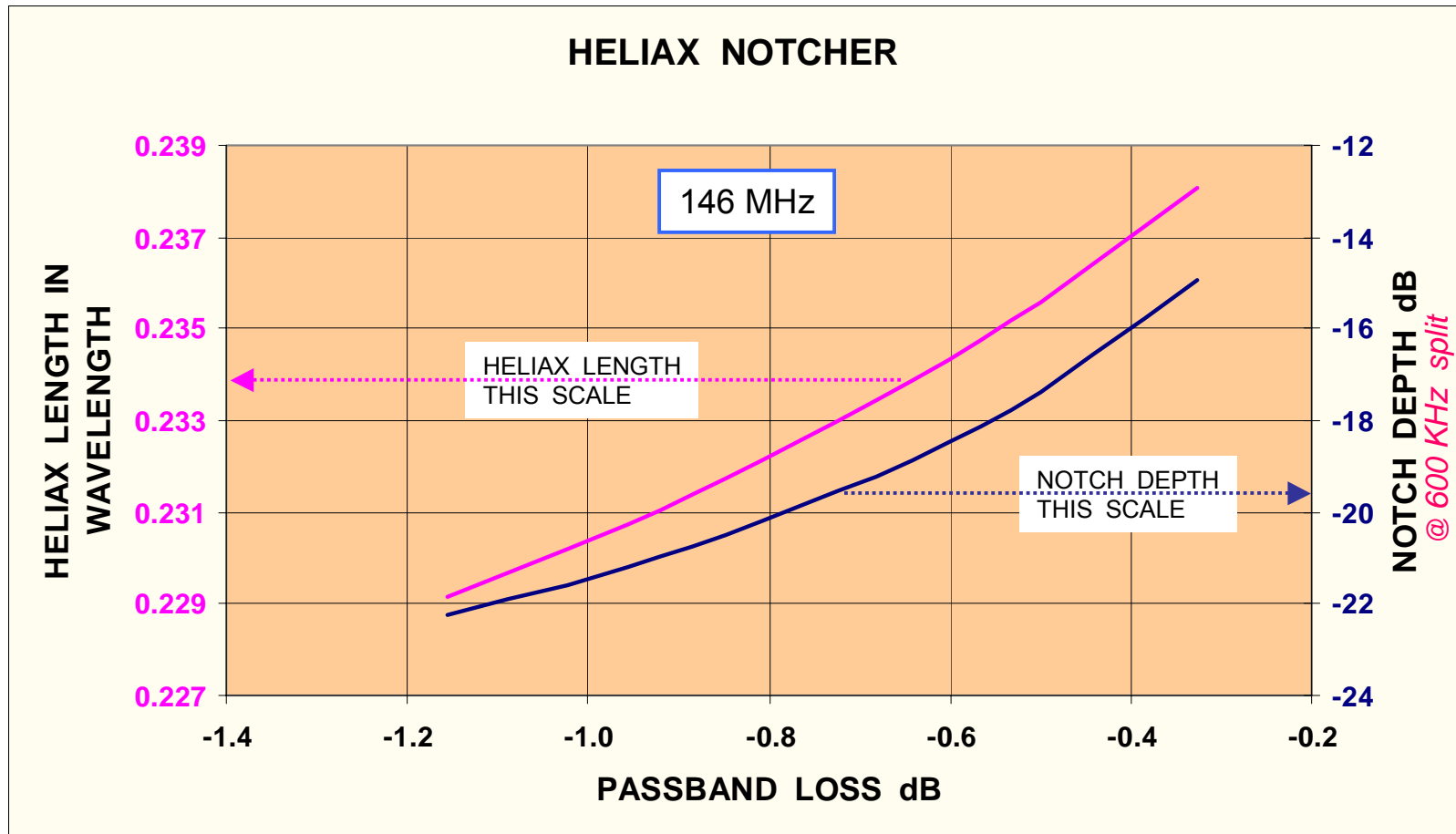
# HELIAX NOTCHER - FREQUENCY RESPONSE

1 5/8 in. FOAM HELIAX  $V_f=0.87$  50 ohms 0.156 dB/100 ft @ 50 MHz  
Series cap = 50 ohm foam coax  $V_f=0.87$  2.2 dB/100 ft @ 150 MHz



# ATTENUATION AND LENGTH DATA FOR THE HELIAX NOTCHER

1 5/8 in. FOAM HELIAX  $V_f=0.87$  50 ohms 0.156 dB/100 ft @ 50 MHz  
Series cap = 50 ohm foam coax  $V_f=0.87$  2.2 dB/100 ft @ 150 MHz



NOTE: Use with a  $\lambda/4$  connecting line. The line adds ~ 5 dB to the notch depth

# COMPARISONS

## CAVITY TYPE

## PLUS

## MINUS

### BANDPASS

- EASIEST TO ADJUST
- INCREASING REJECTION OF OUTSIDE SIGNALS

- POOR REJECTION CLOSE TO BANDPASS  
(12-18 dB @ 600 KHz on 2m)

### DUAL LOOP BANDPASS

- BEST NOTCH DEPTH  
~ 45 dB typical 6" cavity
- ONLY ONE NOTCH
- NOTCH TUNE SENSITIVITY IS LOW: -20% / 100KHz

- FLOATING SERIES CAPACITOR
- SERIES INDUCTOR DIFFICULT TO ADJUST
- SOME REJECTION OUTSIDE BANDPASS

### SERIES RESONANT LOOP

- EASY TO ADJUST VIA SER CAP OR COUPLING
- GOOD NOTCH DEPTH  
~ 37 dB typical 6" cavity

- TWO NOTCHES – MISLEADING
- NOTCH TUNE SENSITIVITY IS HIGH: -1% / 100KHz
- LOOP Q DETERMINES NOTCH DEPTH
- LITTLE REJECTION OUTSIDE BANDPASS AND NOTCH

### PARALLEL RESONANT LOOP (Q circuit)

- SAME AS SERIES RESONANT LOOP

- SAME AS SERIES RESONANT LOOP
- QUARTER WAVELENGTH CABLE INTRODUCE ADDITIONAL LOSSES

### NOTCH CAVITIES

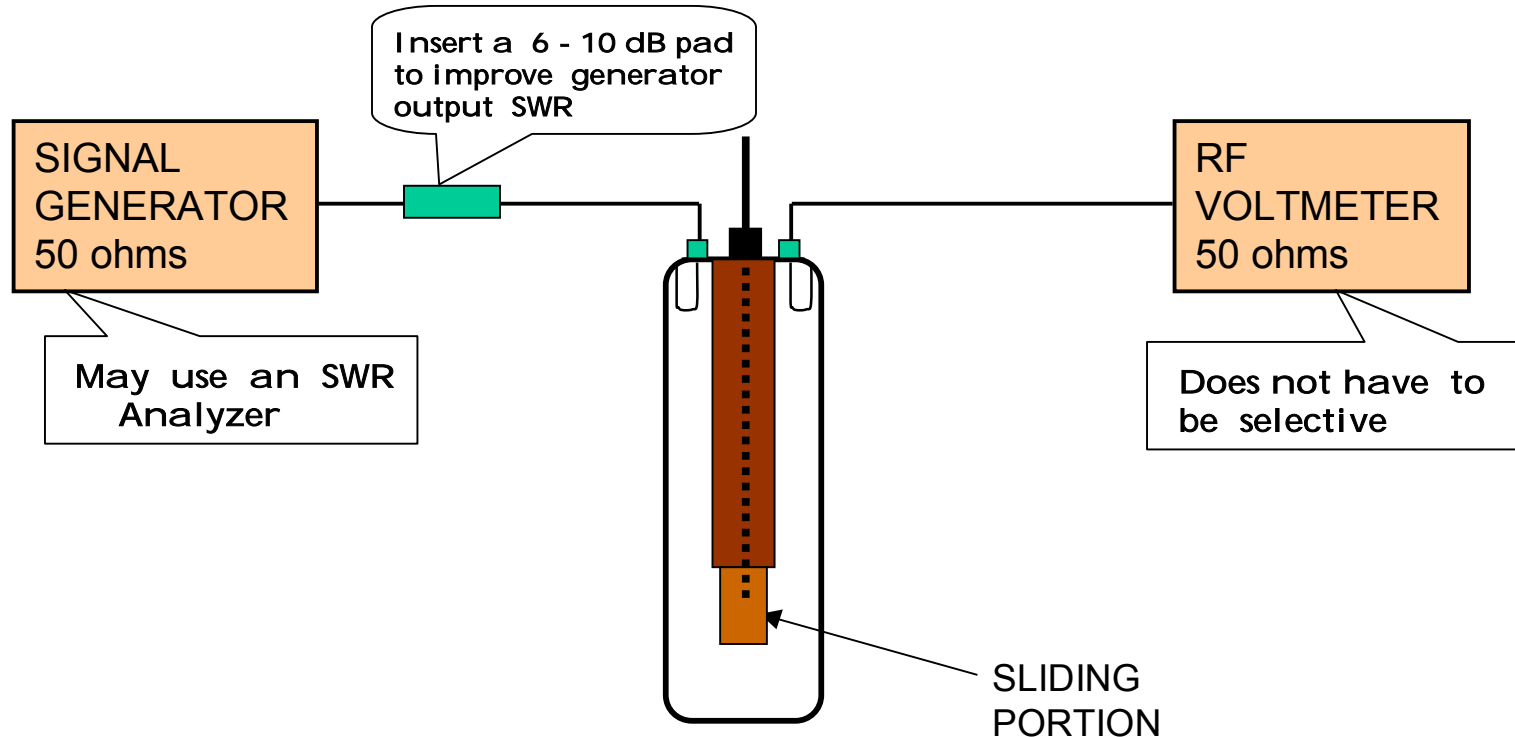
- ATTENUATE A NARROW BAND OF FREQUENCIES
- MAY BE BUILT USING HELIAX CABLE

- NOTCH DEPTH NOT AS GOOD AS IN NOTCH-BANDPASS DESIGNS
- USE WITH BANDPASS CAVITIES TO PROVIDE REJECTION FAR FROM TX/RX

# TUNING INDIVIDUAL CAVITIES

## TUNING BANDPASS CAVITIES

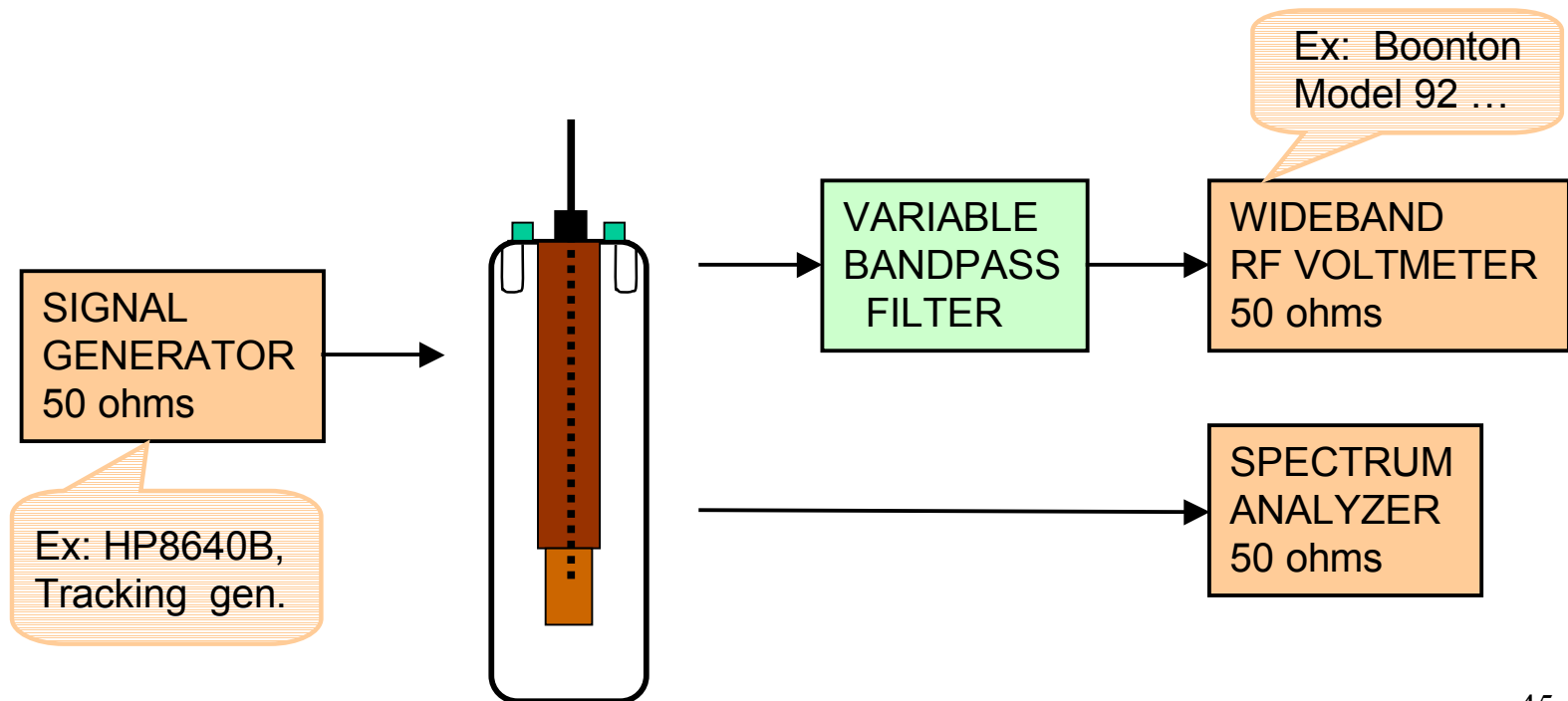
- ❑ ADJUST THE BANDPASS FREQUENCY FOR MAXIMUM SIGNAL
- ❑ CHECK THE INSERTION LOSS. CHANGE THE LOOP COUPLING IF REQ'D



# TUNING NOTCH - BANDPASS CAVITIES

## ABOUT THE VOLTMETER...

- ❑ WIDE BAND VOLTMETERS MAY PICK UP GENERATOR HARMONICS WHEN MEASURING NOTCH DEPTH
- ❑ A SELECTIVE VOLTMETER IS REQUIRED



# TUNING NOTCH - BANDPASS CAVITIES

## DUAL LOOP CAVITIES (MODIFIED BANDPASS TYPES)

- ❑ ADJUST THE BANDPASS FREQUENCY FOR MAXIMUM SIGNAL
- ❑ CHECK THE PASSBAND ATTENUATION AND ADJUST THE LOOP COUPLING AS REQUIRED (typically 0.3 TO 1.5 dB)
- ❑ TO INCREASE THE NOTCH FREQUENCY:  
DECREASE THE NOTCH CAPACITOR OR  
DECREASE THE NOTCH INDUCTOR
- ❑ NOTE THAT NOTCH DEPTH GETS WORSE AS THE NOTCH FREQUENCY GETS CLOSER TO THE BANDPASS FREQUENCY
- ❑ ADJUST THE BANDPASS FREQUENCY FOR LOWEST SWR
- ❑ RECHECK THE INSERTION LOSS AT THE BANDPASS FREQUENCY
- ❑ RECHECK THE NOTCH FREQUENCY AND DEPTH

# TUNING NOTCH - BANDPASS CAVITIES

## SERIES OR PARALLEL LOOP CAVITIES

- ❑ ADJUST THE BANDPASS FREQUENCY FOR MAXIMUM SIGNAL
- ❑ CHECK THE PASSBAND ATTENUATION AND ADJUST THE LOOP COUPLING AS REQUIRED (typically 0.3 TO 1.5 dB)
- ❑ TO INCREASE THE NOTCH FREQUENCY:
  - UPPER NOTCH - ABOVE BANDPASS:
    - DECREASE THE NOTCH CAPACITOR OR INCREASE COUPLING
  - LOWER NOTCH - BELOW BANDPASS:
    - DECREASE THE NOTCH CAPACITOR OR DECREASE COUPLING
- ❑ NOTE THAT NOTCH DEPTH GETS WORSE AS THE NOTCH FREQUENCY GETS CLOSER TO THE BANDPASS FREQUENCY
- ❑ ADJUST THE BANDPASS FREQUENCY FOR LOWEST SWR
- ❑ RECHECK THE INSERTION LOSS AT THE BANDPASS FREQUENCY
- ❑ RECHECK THE NOTCH FREQUENCY AND DEPTH

# NOTCH - BANDPASS CAVITIES

## LOOP RESONANCE VERIFICATIONS - SERIES OR PARALLEL LOOPS

BEST DONE WITH THE LOOP REMOVED FROM THE CAVITY

UPPER NOTCH - ABOVE BANDPASS: (see the graph below)

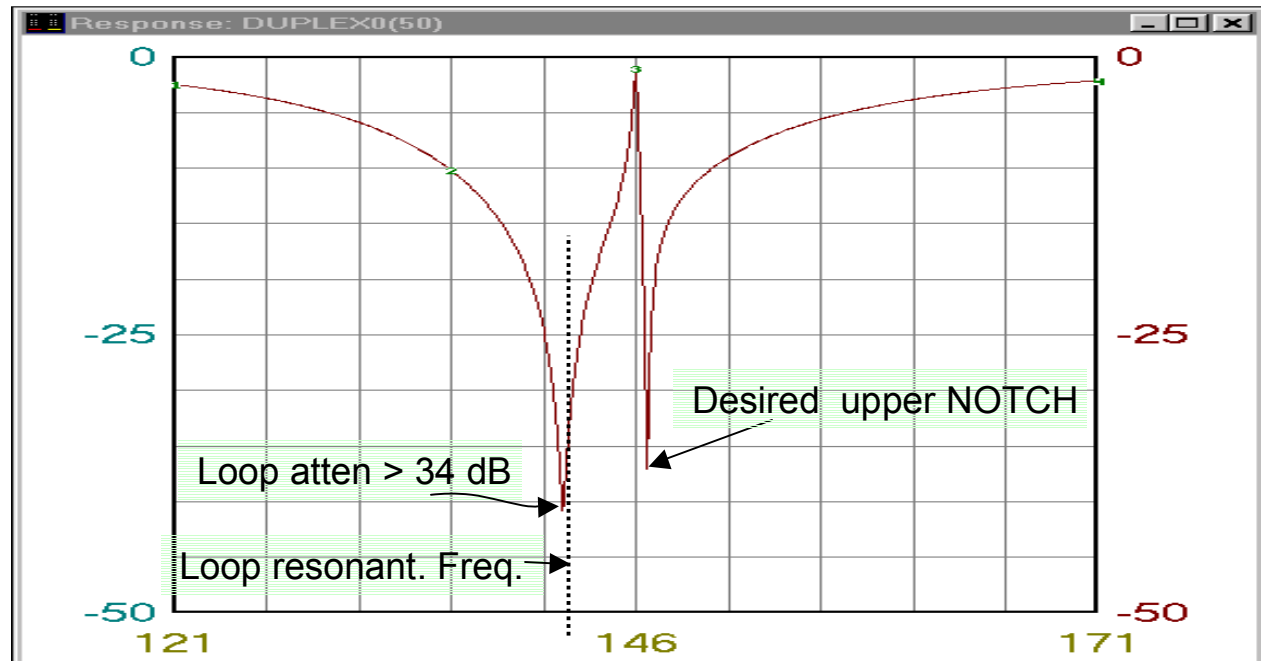
THE LOOP SHOULD RESONATE FROM ~ 130 to 140 MHz

LOWER NOTCH - BELOW BANDPASS:

THE LOOP SHOULD RESONATE FROM ~ 150 to 160 MHz

SHOULD GIVE AT LEAST 34 dB ATTENUATION (IN A 6 in. CAVITY)

AS SHOWN HERE:  
THE LOOP RESONANT  
FREQ. AND ATTEN.  
MAY ALSO BE  
OBTAINED FROM  
THE CAVITY  
RESPONSE





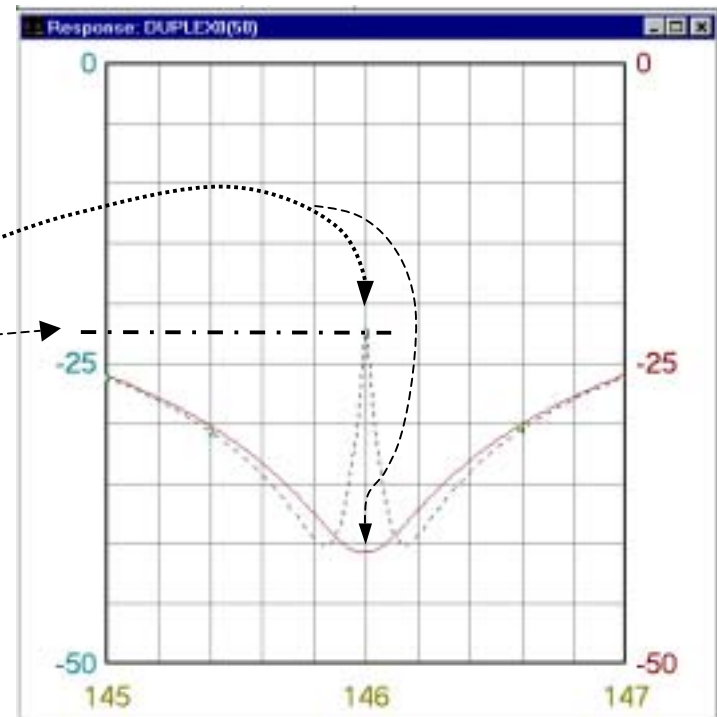
# NOTCH - BANDPASS CAVITIES

## Qu FACTOR VERIFICATION

ADJUST THE RESONATOR AND  
THE LOOP TO RESONATE AT  
THE SAME FREQUENCY

ADJUST THE COUPLING FOR  
~ 20 dB ATTENUATION

MEASURE THE -3 dB FREQUENCIES  
AND CALCULATE  $Q_u$  AS PREVIOUSLY  
DESCRIBED

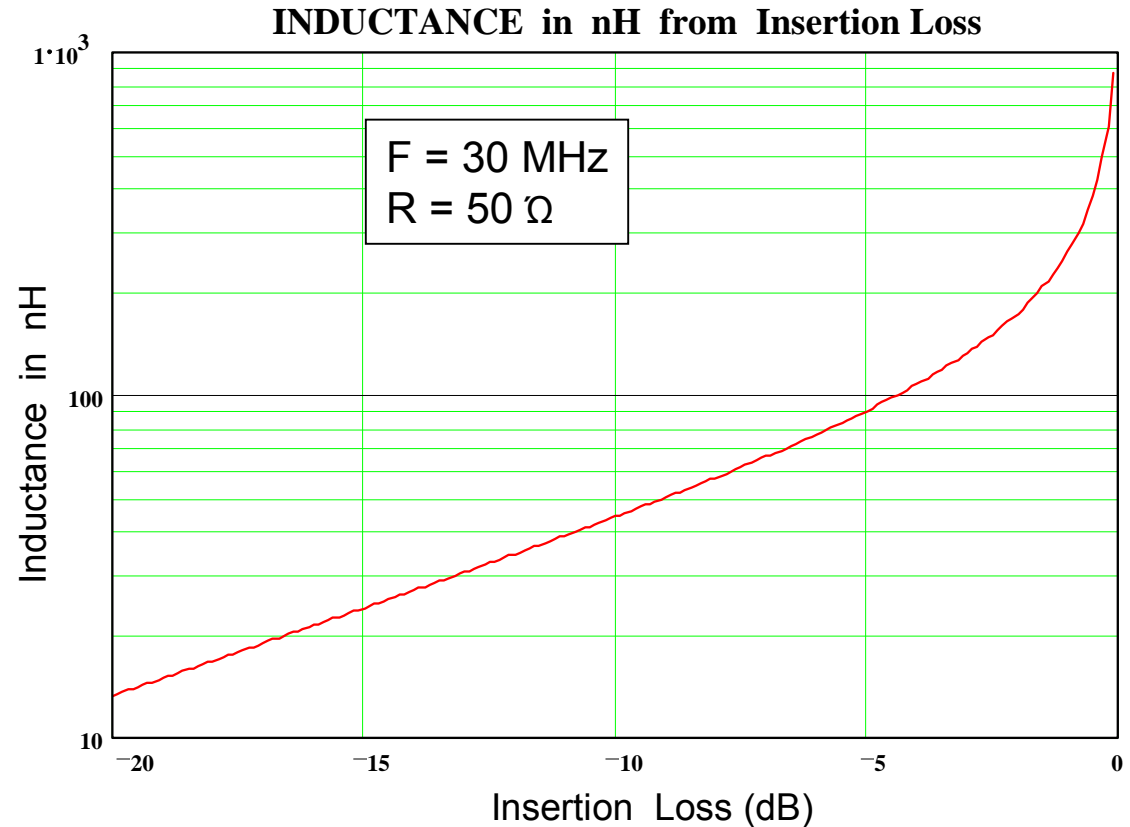


Qu FACTOR VERIFICATION

# MEASURING LOOP INDUCTANCE

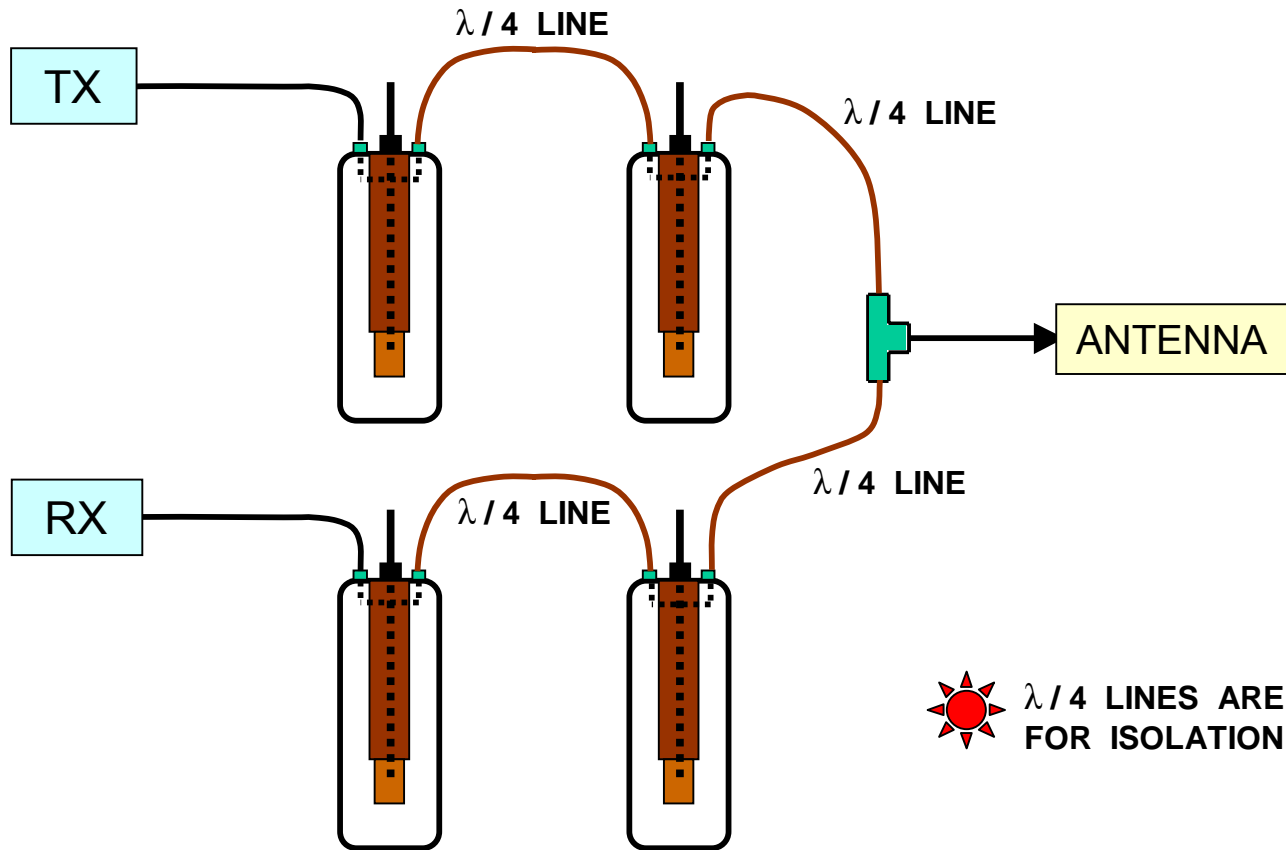
MEASURE THE ATTENUATION IN dB CAUSED BY INSERTING THE LOOP IN A SHUNT CIRCUIT WITH A GENERATOR / DETECTOR IMPEDANCE = R (ohms) AT A FREQUENCY: F in MHz AND COMPUTE THE INDUCTANCE L in nH:

$$L = \frac{79.58 \cdot R \cdot 10^{\frac{\text{dB}}{20}}}{F \cdot \sqrt{1 - \left[10^{\left(\frac{\text{dB}}{20}\right)}\right]^2}} \text{ in nH}$$



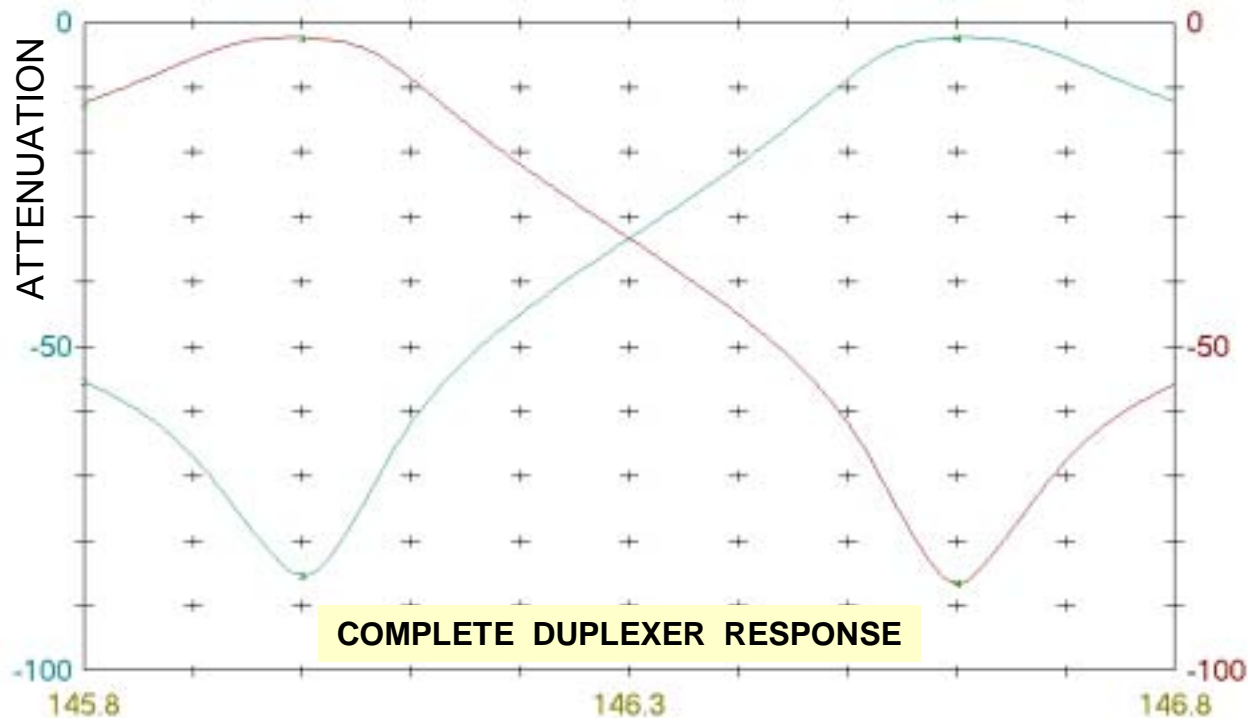
# PUTTING IT ALL TOGETHER

## DUPLEXER BUILT WITH FOUR 6 in. SERIAL LOOP CAVITIES



## EXAMPLE OF DUPLEXER BUILT WITH FOUR 6 in. SERIAL LOOP CAVITIES

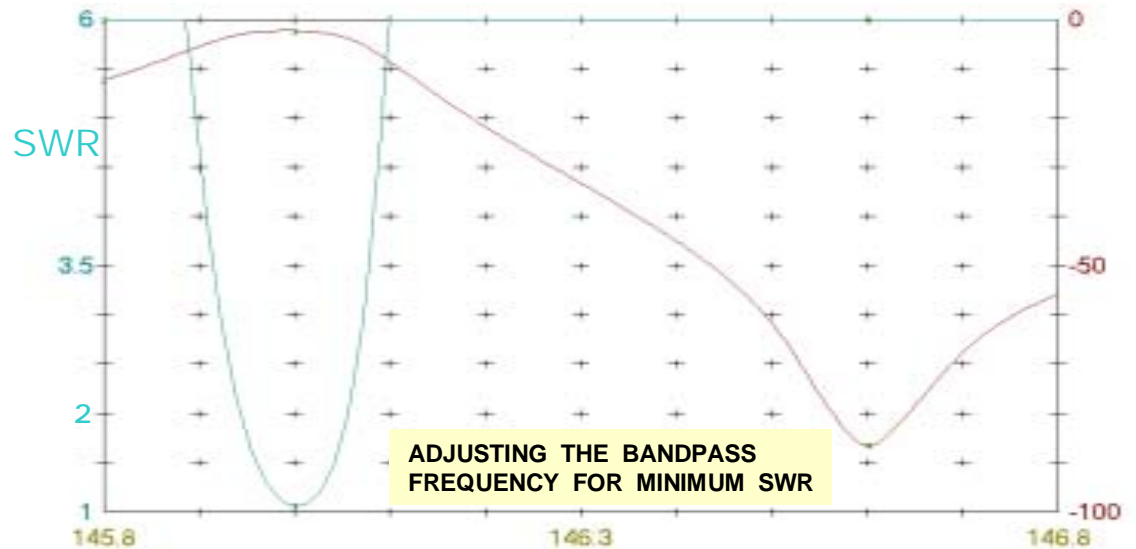
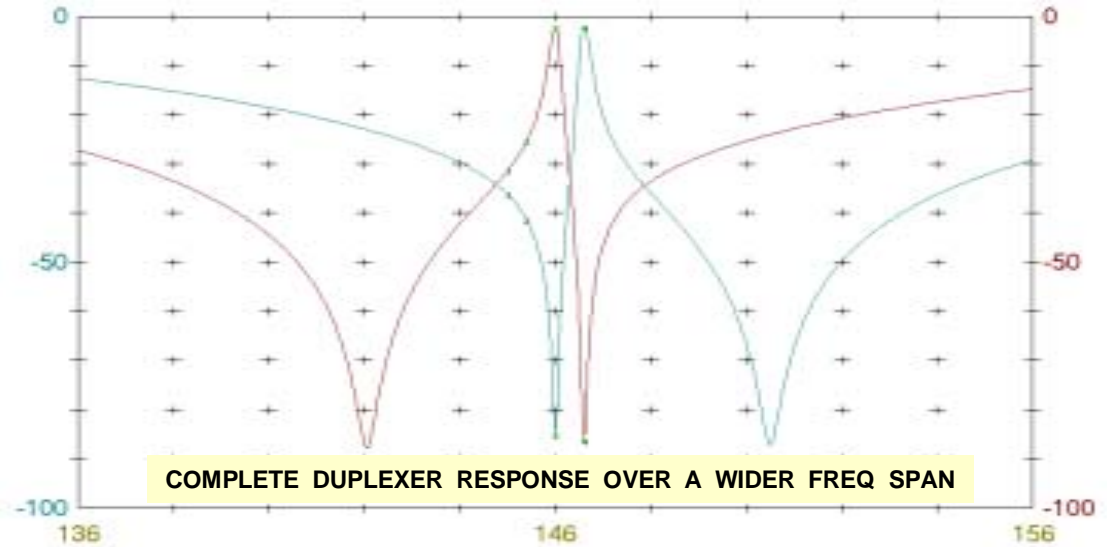
- ❑ BANDPASS INSERTION LOSS: ~ 2.2 Db (1 dB PER CAVITY +  $\lambda/4$  LINE LOSSES)
- ❑ NOTCH DEPTH: ~ 85 dB
- ❑ NOTCH DEPTH = ~ SUM OF NOTCH DEPTH OF EACH CAVITY + 5.5 dB **PER**  $\lambda/4$  LINE  
Example: NOTCH DEPTH = 37 dB + 37 dB + 5.5 x 2 cables = 85 dB



# EXAMPLE OF DUPLEXER BUILT WITH FOUR 6 in. SERIAL LOOP CAVITIES

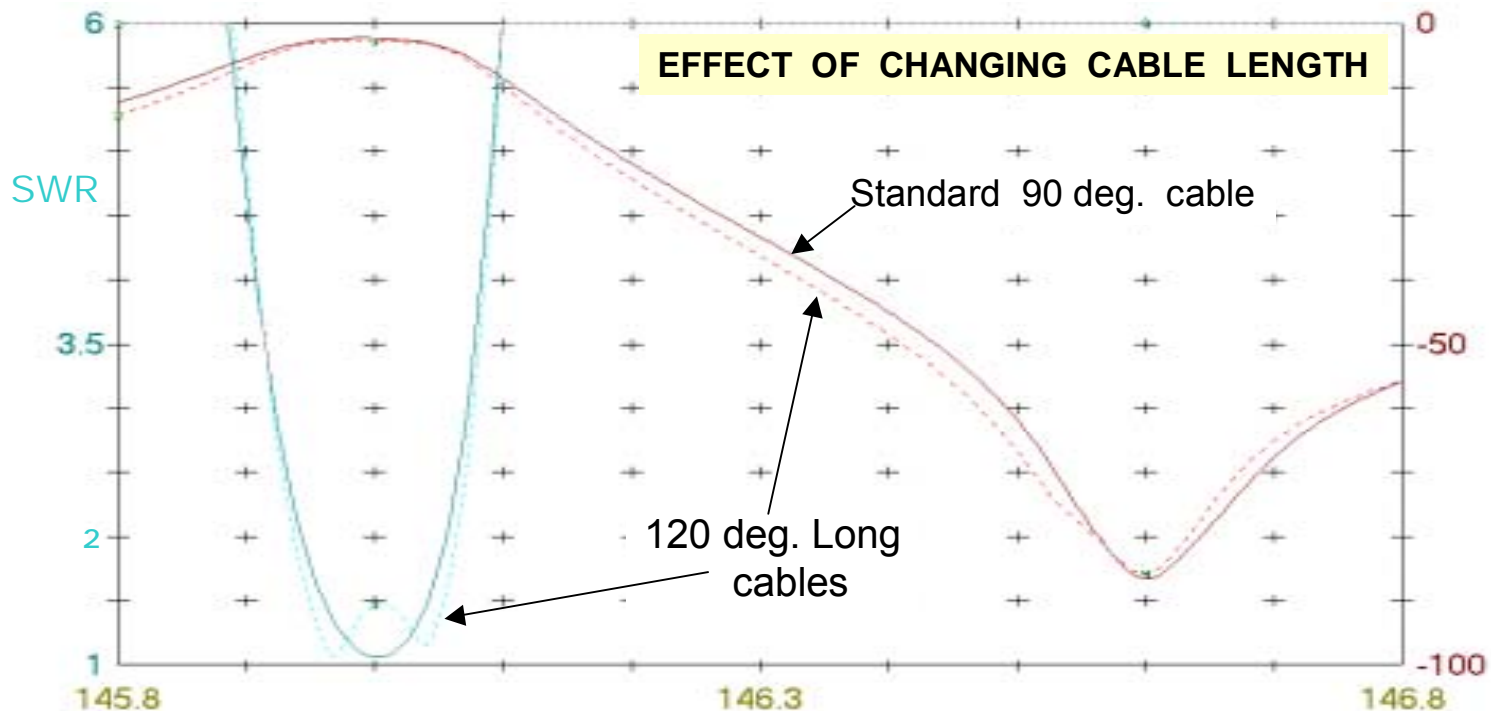
- ❑ THIS TYPE OF DUPLEXER PROVIDES LITTLE REJECTION OF OUT OF BAND SIGNALS

- ❑ ADJUSTING THE BANDPASS FREQUENCY FOR MINIMUM SWR IS BEST
- ❑ MAY REQUIRE ABILITY TO READ LOW SWR VALUES



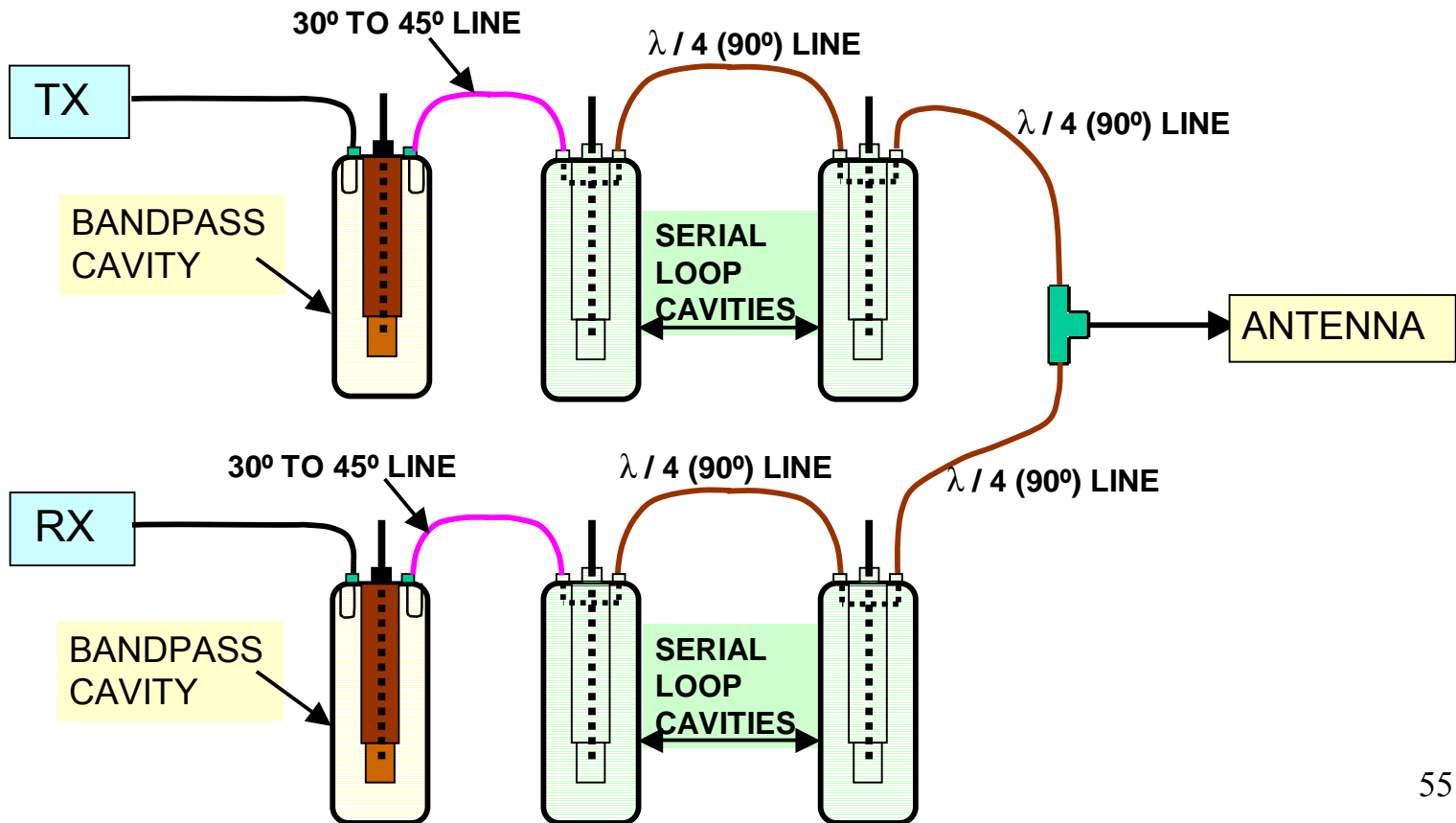
## EXAMPLE OF DUPLEXER BUILT WITH FOUR 6 in. SERIAL LOOP CAVITIES

- ❑ THE  $\lambda/4$  CABLES AT THE TEE JUNCTION HAVE BEEN INCREASED IN LENGTH 33%
- ❑ SLIGHT CHANGE IN RESPONSE
- ❑ SWR CURVE HAS RIPPLES NOW. THIS MAY BE USED TO CHECK FOR PROPER CABLE LENGTHS



## EXAMPLE OF DUPLEXER BUILT WITH TWO BANDPASS + FOUR SERIAL LOOP CAVITIES

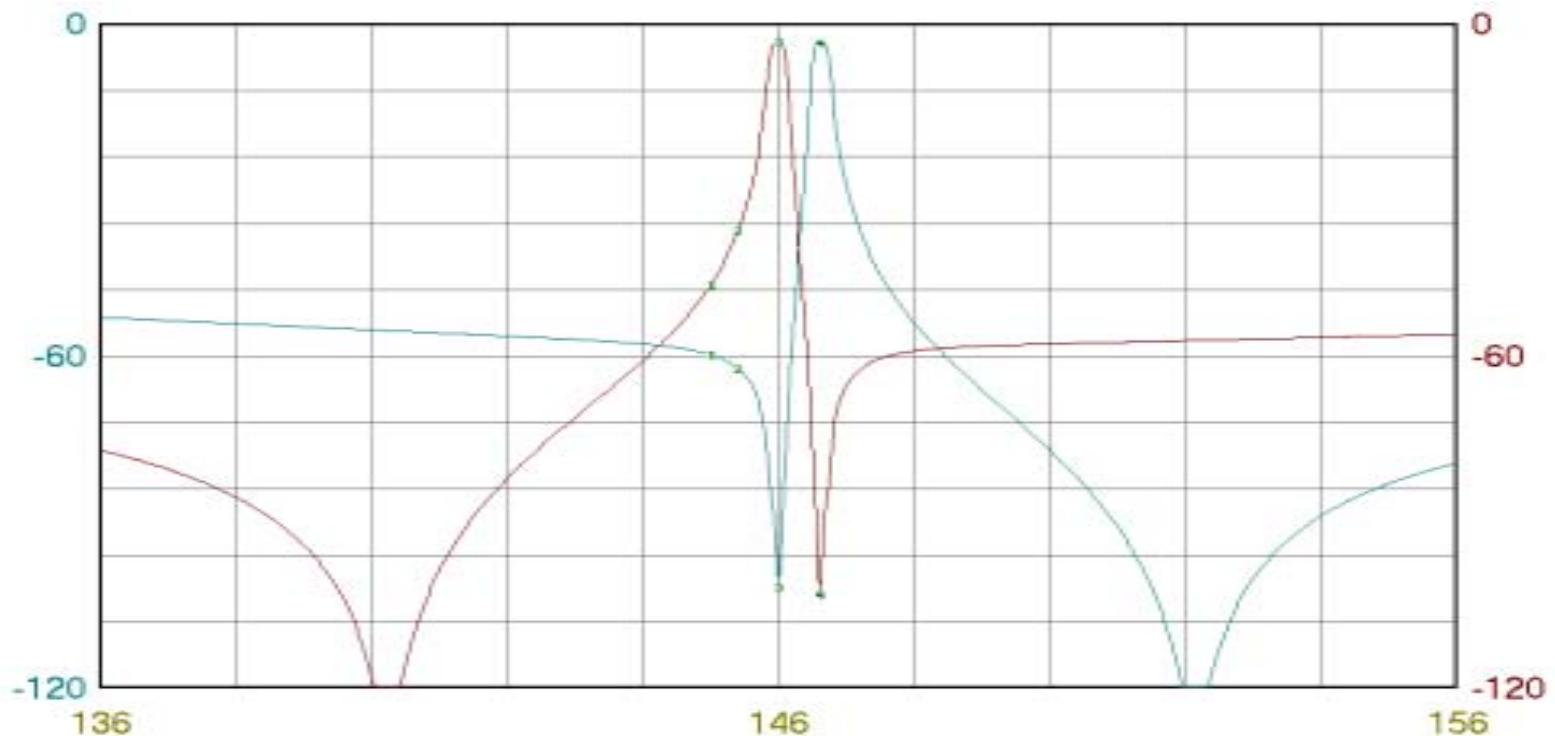
- ❑ BANDPASS CAVITIES SHOULD BE PLACED AHEAD OF SERIAL LOOP CAVITIES
- ❑ THE 30° TO 45° LINE AFTER THE BANDPASS CAVITIES ADDS ~ 5dB NOTCH DEPTH
- ❑ IMPROVES REJECTION



## EXAMPLE OF DUPLEXER BUILT WITH TWO BANDPASS + FOUR SERIAL LOOP CAVITIES

FEATURES:

- 3 dB BANDPASS LOSS (~ 1dB per cavity)
- ~102 dB NOTCH
- EXCELLENT REJECTION OF OUT OF BAND SIGNALS



COMPLETE DUPLEXER RESPONSE OVER A 20 MHz FREQ SPAN



## PITFALLS

### ❑ AVOID LOW QUALITY CONNECTORS SPECIALLY TEES.

The picture on the right shows an N type connector that uses a steel spring for making contact with the thru line. The added inductance was calculated from return loss measurement at 100 MHz (9.5 dB) and 1 GHz (5 dB) with both female ends terminated (50 ohms) This gave  $\sim 7$  nH inductance. Therefore a 100 nH loop will have its inductance increased by 7%, thus lowering its resonant frequency 3.5% or  $\sim 5$  MHz at 146 MHz !

### ❑ USE SILVER PLATED CONNECTORS

❑ UNPLATED COPPER CAVITIES MAY BE POLISHED AND CLEANED WITH “BRASSO” (liquid copper / brass cleaner) LEAVES A PROTECTIVE FILM

❑ SLIDING CONTACTS MAY BE LUBRICATED WITH SILICONE CLEANER OR VASELINE

❑ TERMINATE THE “UNUSED” PORT WHEN TESTING FOR LOSS OR SWR

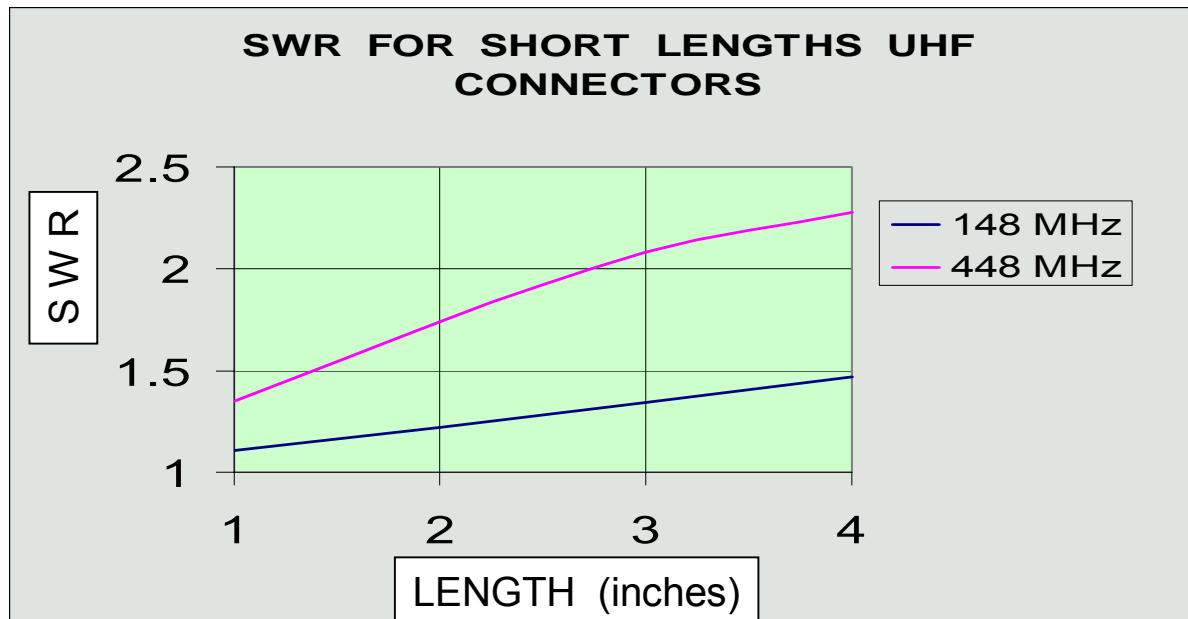


N Type Tee

CENTER CONNECTOR  
USES A SPRING FOR  
CONTACT !

## PITFALLS

- ❑ TEMPERATURE SENSITIVITY:  
UNCOMPENSATED Cu RESONATORS WILL SHOW  
A TEMPERATURE COEFFICIENT OF  $\sim -1.3$  KHz / degC (146 MHz)
- ❑ DOUBLE SHIELD CABLES AND N TYPE CONNECTORS PREFERRED
- ❑ AVOID – IF POSSIBLE - UHF ADAPTERS  
THEIR IMPEDANCE IS BELOW 50 OHMS:  $\sim 33$  OHMS  
THEY WILL LIKELY INCREASE THE SWR



## CONCLUSION

- ❑ THIS PRESENTATION COVERS THE MOST IMPORTANT DUPLEXER ELEMENTS:  
BANDPASS + 3 TYPES OF NOTCH – BANDPASS + NOTCH DESIGNS
- ❑ SIMULATION SOFTWARE WITH REAL TIME TUNING CAPABILITIES ALLOWS « BREADBOARDING » DUPLEXERS
- ❑ LEARN TUNING, CHECK FOR SENSITIVITY TO COMPONENT VARIATIONS SUCH AS Q FACTOR, CABLE LENGTHS ETC.

## REFERENCES

- ❑ LINEAR SIMULATION SOFTWARE:
  - SuperStar from Eagleware (used here)
  - Serenade SV for Windows from Ansoft (free)
  - ARRL Radio designer from ARRL
  - Pspice Student version
  
- ❑ Duplexer Theory and Testing by Dave Metz WA0UAQ (.pdf format)
  
- ❑ KI7DX 6 Meter Repeater [http://www.wa7x.com/ki7dx\\_rpt.html](http://www.wa7x.com/ki7dx_rpt.html)
  
- ❑ 6 Meter Heliax Duplexers <http://www.dallas.net/~jvpoll/dup6m/dup6m.html>
  
- ❑ Duplexers: theory and tune up <http://www.seits.org/duplexer/duplexer.htm>
  
- ❑ Upgrading Boonton Models 92/42 RF Voltmeters Jacques Audet  
Communications Quarterly Spring 97
  
- ❑ THANKS to Jean-Nicol VE2BPD for the photos and the bad tee